



**McCLYMONT & RAK**  
ENGINEERS, INC.  
GEO-ENVIRONMENTAL CONSULTANTS

WWW.MCCRAK.COM

111 ZENWAY BLVD., UNIT 4, VAUGHAN, ONTARIO, L4H 3H9  
TEL: 416.675.0160 FAX: 905.851.1722  
office@mccrak.com

1271 DENISON ST., UNIT 45, MARKHAM, ONTARIO, L3R 4B5  
TEL: 905.470.0160 FAX: 905.475.6371  
denison@mccrak.com

McMASTER INNOVATION PARK - COLABORATORY No. 110A  
175 LONGWOOD RD. S., HAMILTON, ONTARIO, L8P 0A1  
office@mccrak.com



**MG4842**

**MARCH 2021**

**PRELIMINARY GEOTECHNICAL REPORT  
PROPOSED  
RESIDENTIAL/COMMERCIAL DEVELOPMENT  
PIER 27, PHASE 3  
BUILDINGS A AND F  
25 & 35 QUEENS QUAY EAST  
TORONTO, ONTARIO**

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**PREPARED FOR:**

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PIER 27 TORONTO (NORTHEAST) INC.  
56 THE ESPLANADE, SUITE 308  
TORONTO, ONTARIO  
M5E 1A7

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## 1.0 INTRODUCTION

Pier 27 Toronto (Northeast) Inc. (the Client) retained MCR to prepare a geotechnical report for the proposed residential/commercial development (Pier 27 North ) located at Queens Quay East and Yonge Street, Toronto, Ontario (hereafter referred to as 'the Site').

The objective of the report was to determine design data required for foundations, dewatering, shoring/excavation, backfill, slab on grade, and pavement. The above design and construction issues are addressed in the following report.

## 2.0 SITE CONDITION

The Site is located on the southeast corner of the intersection of Queens Quay East and Yonge Street, in Toronto, Ontario. The rectangular shaped site is currently an asphalt paved parking lot in the western portion, with a sales centre in the northeast and construction storage (for Phase II of the development) in the southeast portion.

Queens Quay East limits the subject site to the north, Yonge Street to the west and residential developments to the east and south. The ground surface is relatively flat with a slight slope towards the west.

### 2.1 PROPOSED DEVELOPMENT

The proposed redevelopment includes a forty five [45] storey tower with an eleven [11] storey podium (Building F), and an eleven [11] storey building (Building A), over four [4] levels of below grade parking.

The finished floor elevation (FFE) at ground level is expected to be at an elevation of 77.30 m. The lowest P4 FFE will be at an elevation of 63.24 m (Appendix A).

### 3.0 SITE INVESTIGATION

Twelve [12] boreholes (BH 20-1 to BH 20-8) were drilled, by MCR, at the subject site from September 21 to 25, 2020, at locations shown on Drawing No. 1. The boreholes were advanced to depths ranging from 3.96 to 14.02 m. The borehole records are enclosed in Appendix B.

Monitoring wells were installed in all boreholes, except 20-3, 20-4 and 20-7 for long-term groundwater monitoring and sampling.

The geodetic elevations of the boreholes were surveyed by MCR, and referenced to a temporary bench mark established by Krcmar on September 16, 2020, with a reported elevation of 77.43 masl.

### 4.0 SOIL AND GROUNDWATER CONDITIONS

Subsurface conditions, encountered at borehole locations, are shown on Borehole Log Sheets attached in Appendix B and summarized as follows:

**Pavement:** An asphalt layer, 75 mm in thickness, was observed at the surface of boreholes 20-4, 20-5-D and 20-7 and a 75 mm thick concrete layer was present at the surface of borehole 20-8. Granular fill, varying from 425 to 525 mm in thickness, underlies the asphalt/concrete in the boreholes.

**Fill:** Loose to compact fill consisting of sand, silt, gravel and clay/clayey silt was present at the surface of boreholes 20-1-D, 20-2, 20-3 and 20-6-D and below the pavement at boreholes 20-4, 20-5-D, 20-7 and 20-8. The moist to wet fill contained trace clay, sand, gravel and clinker, trace to some organics, and debris such as decayed wood and brick fragments. The brown to black fill extended to depths ranging from 4.27 to 6.10 m.

**For the purpose of offsite disposal, the type/quantity and extent of the existing fill/organic materials/granular fill layers should be explored by further test pit investigation, prior to contract award.**

**Sand:** A layer of very loose to loose, medium to fine sand was detected below the fill at boreholes 20-1-D and 20-8 and extended to the depths of 6.10 and 5.20 m, respectively. The dark brown to black sand contained some silt and trace gravel and was in a wet condition.

**Silt/Silty Clay/Sandy Silt:** A layer of soft to hard silt/silty clay/sandy silt was encountered below fill/sand at all boreholes except 20-1-S, 20-5-S, 20-8 and 20-6-S. The deposit was in a moist to wet condition and contained trace to some sand, trace gravel, shells, clay and organics. Dark brown to black and black to grey silt/silty clay/sandy silt extended to the depths ranging from 5.18 to 12.50 m.

Although no boulders were encountered during the geotechnical investigation, using 100 to 150 mm diameter boreholes, the substructure is to be constructed in soils that went through historic periods of glaciation. As a result, glacial drop stones, ranging from gravel to boulders can be encountered within the overburden.

**Shale:** Grey moist shale was found below silty clay at boreholes 20-1-D, 20-5-D and 20-6-D at depths ranging from 11.89 to 13.41 m and extended to the maximum depth of boreholes at depths ranging from 12.65 to 14.02 m, at elevations 63.01 to 65.41 m.

**Groundwater:** Upon completion of drilling all the boreholes remained dry.

The groundwater level was measured, in the installed wells, on six occasions between September 28 to October 19, 2020 at depths varying from 2.25 to 11.64 m. The results are summarized in Table 1.

**Table 1 – Groundwater Level Monitoring Results**

Monitoring Well Id	Ground Surface Elevation (masl)	Water Level (mbgs)	Groundwater Elevation (masl)	Date of Measurement (mm/dd/yyyy)	Depth of Well (mbgs)	Depth of Bentonite (mbgs)	Length of Screen (m)	Inside Diameter of Pipe (mm)	Top of Monitoring Well
20-1-S	76.93	2.55	74.38	09/28/2020	3.96	0.30	3.05	50	FLUSH MOUNT
		2.58	74.35	10/01/2020					
		2.61	74.32	10/05/2020					
		2.62	74.31	10/09/2020					
		2.59	74.34	10/14/2020					
		2.64	74.29	10/19/2020					
20-1-D	76.93	11.29	65.64	09/28/2020	12.19	9.75	3.05	50	FLUSH MOUNT
		7.50	69.43	10/01/2020					

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		7.54	69.39	10/05/2020					
		7.52	69.41	10/09/2020					
		7.50	69.43	10/14/2020					
		7.50	69.43	10/19/2020					
20-2	76.08	2.71	73.37	09/28/2020	4.57	0.91	3.05	50	FLUSH MOUNT
		2.69	73.39	10/01/2020					
		2.72	73.36	10/05/2020					
		2.72	73.36	10/09/2020					
		2.70	73.38	10/14/2020					
		2.78	73.30	10/19/2020					
20-5-S	77.03	2.55	74.48	09/28/2020	4.27	0.60	3.05	50	FLUSH MOUNT
		2.56	74.47	10/01/2020					
		2.55	74.48	10/05/2020					
		2.57	74.46	10/09/2020					
		2.58	74.45	10/14/2020					
		2.56	74.47	10/19/2020					
20-5-D	77.03	11.29	65.74	09/28/2020	13.41	9.45	3.05	50	FLUSH MOUNT
		11.40	65.63	10/01/2020					
		11.26	65.77	10/05/2020					
		11.55	65.48	10/09/2020					
		11.20	65.83	10/14/2020					
		11.64	65.39	10/19/2020					
20-6-S	77.06	2.66	74.40	09/28/2020	9.14	5.49	3.05	50	FLUSH MOUNT
		2.66	74.40	10/01/2020					
		3.36	73.70	10/05/2020					
		2.73	74.33	10/09/2020					
		2.69	74.37	10/14/2020					
		2.69	74.37	10/19/2020					
20-6-I	77.06	2.84	74.22	09/28/2020	4.57	0.60	3.05	50	FLUSH MOUNT
		2.89	74.17	10/01/2020					
		2.90	74.16	10/05/2020					
		2.90	74.16	10/09/2020					
		2.82	74.24	10/14/2020					
		2.83	74.23	10/19/2020					
20-6-D	77.06	9.80	67.26	09/28/2020	12.19	9.75	3.05	50	FLUSH MOUNT
		9.82	67.24	10/01/2020					
		10.00	67.06	10/05/2020					
		9.83	67.23	10/09/2020					
		9.80	67.26	10/14/2020					
		9.84	67.22	10/19/2020					
20-8	77.05	2.25	74.80	09/28/2020	4.57	0.91	3.05	50	FLUSH MOUNT
		2.28	74.77	10/01/2020					
		2.26	74.79	10/05/2020					
		2.26	74.79	10/09/2020					
		2.25	74.80	10/14/2020					
		2.27	74.78	10/19/2020					
Min	76.08	2.25	65.39	-	3.96	-	-	-	-
Max	77.06	11.64	74.80	-	13.41	-	-	-	-
Average	76.91	5.02	71.89	-	7.65	-	-	-	-

It should be noted that groundwater levels are subject to seasonal fluctuations. Consequently, definitive information on the long-term groundwater levels could not be

obtained during this study.

In addition, Geohydrology assessment study is currently underway. The results of the assessment will be presented in a separate report.

It is recommended that, as a minimum, prior to the design of the dewatering system, a pumping test be carried out.

## 5.0 FOUNDATION

The proposed redevelopment includes a forty five [45] storey tower with an eleven [11] storey podium (Building F), and an eleven [11] storey building (Building A), over four [4] levels of below grade parking.

The finished floor elevation (FFE) at ground level is expected to be at an elevation of 77.30 m. The lowest P4 FFE will be at an elevation of 63.24 m (Appendix A).

Based on the encountered soil/rock foundation conditions, the proposed development with four underground parking levels can be supported on conventional spread/strip footings.

The proposed footings could be proportioned using the following bearing resistance:

Factored Bearing Resistance at ULS = 3500 kPa

Bearing Resistance at SLS = 2500 kPa

When established in weathered shale bedrock, at least 300 mm below the surface of shale bedrock, at or below an approximate elevation ranging from 63.30 to 64.75 m, subject to final design grades, the depth of shale bedrock across the site, to be confirmed by further onsite borehole investigation, and field inspection during foundation installations.

Coefficient of Subgrade Reaction  $k$  (for sound shale) = 120 MN/m<sup>3</sup> is considered applicable.



## 5.1 GENERAL FOUNDATION NOTES

It is recommended that excavation and construction contract provisions include unit prices for excavation into wet soils which may contain old near shore structures, cobbles, boulders and erratic rock to minimize potential unexpected extra costs during excavation and foundation installations.

Adjacent footings, founded at different elevations, preferably are to be stepped at 10 horizontal to 7 vertical, subject to rock condition during excavations.

For frost protection requirements, the exterior footings and footings in unheated areas in unheated P4 areas must have a minimum shale bedrock cover of 0.5 m.

Any water or loose materials must be removed from the footing bases prior to placing the concrete.

The recommended resistance at SLS allows for up to 25 mm of total settlement. Potential differential settlements are to be evaluated after completion of the foundation drawings.

Furthermore, the recommended bearing resistance and foundation elevations have been calculated from the limited borehole information and are intended for design purposes only.

More specific information with respect to rock/foundation conditions will be available when the proposed shoring/foundation construction is underway. Therefore, the encountered rock/foundation conditions must be verified in the field, and all drilled foundations/footings must be inspected and approved by our office prior to placement of concrete.

## 6.0 EARTHQUAKE CONSIDERATION

The building must be designed to resist a minimum earthquake force. The National Building Code specifies that the building be designed to withstand a minimum lateral seismic force,  $V$ , which is assumed to act non-currently in any direction on the building

as per the following expression:

$$V = S(T_a) M_v I_E W / R_d R_o$$

It should be noted that V shall not be less than:

$$S(2.0) M_v I_E W / R_d R_o$$

In addition, the SFRS (Seismic Force Resisting System (s)) with  $R_d$  equal to or greater than 1.5, V should not be greater than:

$$2/3 S(0.2) I_E W / R_d R_o$$

Where  $S(T_a)$  shall be calculated by  $S_a(T_a)F_a$  or  $S_a(T_a)F_v$ , depending on fundamental lateral period  $T_a$ . The terms, which are relevant to the geotechnical conditions at the site, are acceleration-based site coefficient  $F_a$  and velocity-based site coefficient  $F_v$ .

For the subject site, which is classified as Class B (based on the borehole information), the applicable values of  $F_a$  and  $F_v$  are 0.8 and 0.6 respectively. A structural consultant should review all factors.

## 7.0 BASEMENT WALLS

Basement walls should be designed to resist a pressure "p", at any depth, "h" below the surface, as given by the expression:

$$p = 0.40[\gamma h + q]$$

Where: 0.40 is the earth pressure coefficient considered applicable  
 $\gamma = 21.7 \text{ kN/m}^3$  is the unit weight of backfill  
 $q$  = an allowance for surcharge.

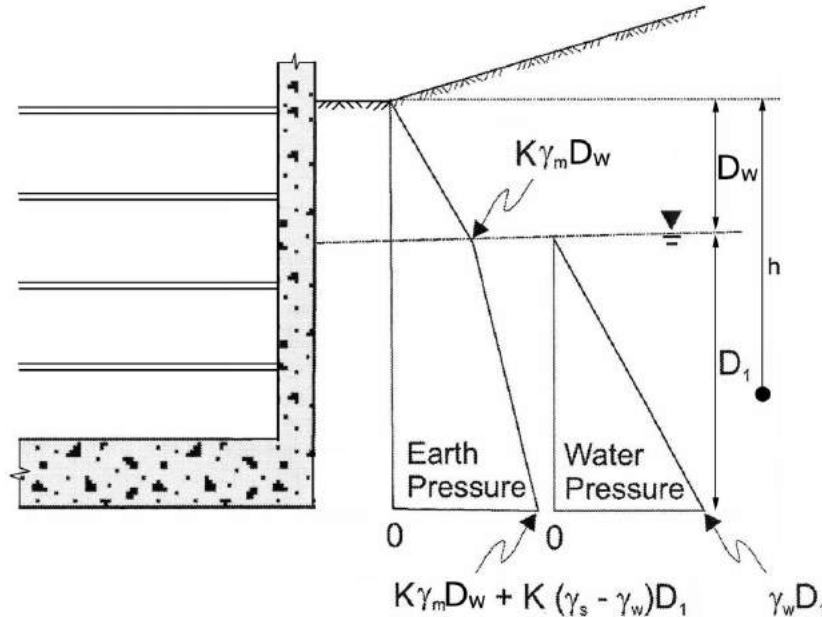
The above equation assumes that perimeter drains will be provided and that the backfill against subsurface walls, where applicable, would be a free draining granular material.

However, subject to groundwater conditions and the presence of the wet silt/silty clay/sandy silt soils, all subject to further groundwater monitoring results, we suggest that perimeter walls below the groundwater level be designed for hydrostatic pressure to resist a pressure "p", at any depth "h" below the surface, as given by the expression:

$$p = \begin{cases} Kq + K\gamma_m h & h \leq D_w \\ Kq + K\gamma_w D_w + K(\gamma_s - \gamma_w)(h - D_w) + \gamma_w(h - D_w) & h > D_w \end{cases}$$

Where:

- $K = 0.50$  is the earth pressure coefficient considered applicable
- $\gamma_m = 20 \text{ kN/m}^3$  is moist or wet soil unit weight
- $\gamma_s = 21.7 \text{ kN/m}^3$  is saturated soil unit weight
- $\gamma_w = 9.80 \text{ kN/m}^3$  is the unit weight of water
- $q$  = an allowance for surcharge.



## 8.0 DEWATERING

The excavation for the proposed underground parking structure will extend through the wet/saturated clayey silt/silty clay/sandy silt soils into bedrock, to a depth below water table.

In order to protect the excavation from being disturbed by excess groundwater pressure, positive dewatering, such as eductors will be required for the proposed excavation.

To control potential localized groundwater influx, upon completion of general excavation, bedrock should be trenched and temporary sump pumps installed.

The selected dewatering system, which should be designed and installed by a specialty contractor, will be most effective if it is activated at the earliest opportunity during/prior to the general excavation.

In addition, a pre-construction survey of the adjacent structures/roads should be carried out prior to the dewatering/shoring construction stage. Potential adverse effects on adjacent structures, due to the dewatering must be assessed/quantified, and suitable preventive/remedial measures implemented.

## 9.0 EXCAVATION AND BACKFILL

No major problems will be encountered for the anticipated depth of general excavations, carried out within a shoring wall enclosure. The excavation in weathered shale bedrock can be carried out with a heavy-duty backhoe.

**However, the shoring/foundation contractor must be aware that the relatively harder limestone slabs or seams are interbedded in the shale bedrock.**

A dewatering system such as eductors will be required for excavation below the groundwater level.

The material to be used for backfilling under floor slab should be size 19 mm clear stone. In service trenches, the fill should be suitable for compaction, i.e. free of

limestone fragments of a size greater than 150 mm, and with natural moisture content, which is within 2 percent of the optimum moisture content. The backfill material should be compacted to at least 98 percent of the Standard Proctor Maximum Dry Density (SPMDD).

The backfill against subsurface walls, where applicable, should be free draining granular fill, preferably conforming to the Ontario Provincial Standard Specification for granular base course, Granular B.

## 10.0 SHORING

A shoring system should be designed to protect adjacent structures and services. The fourth edition of the Foundation Manual should be referred to for the design of the shoring system.

It should be noted that groundwater and boulders will be encountered during soldier pile/caisson construction, and the contractor must be prepared to deal with boulders and water seepage into the caisson shafts without undue delays.

**Specifically, the shoring contractor may experience difficulties during the drilling the much harder limestone slabs.**

Due to the groundwater and wet silt/silty clay/sandy silt soils or perched water in the fill layer, it might be difficult to prevent groundwater from penetrating into the excavation through gaps in timber lagging.

The geotechnical parameters, considered applicable for the design, are as follows:

Active earth pressure coefficient  $K_a = 0.45$  for walls in areas where structures or sensitive services are being supported.

Active earth pressure coefficient  $K_a = 0.28$  for remaining areas.

Natural unit weight of soil =  $21.7 \text{ kN/m}^3$

Passive pressure coefficient in shale bedrock  $K_p = 5$

Any surcharge loads must be included in the lateral pressure calculations.

Lateral movements of the shoring wall, designed using  $K_a = 0.28$ , are expected to be in order of 15 mm. They are expected to be less if  $K_a$  value of 0.45 is used. The expected movements are based on a properly constructed system.

The horizontal and vertical movements should be monitored during construction to ensure satisfactory performance of the shoring system.

Soil and rock anchors should be designed for 20 kPa and 600 kPa, respectively. **It is re-iterated that subsurface conditions may vary beyond the site's confines. As a result, the design values must be confirmed by at least two load tests, carried out to twice the design load.**

It is imperative that a stability analysis of the entire support system is undertaken prior to commencement of construction. The final shoring design should be reviewed by our office.

Space and groundwater influx permitting, lowest parking level could be excavated "neat" into the rock face. A sufficient rock bench/rock bolts will be required to secure the integrity of the shoring system.

The exposed rock face could be shotcreted (if required), subject to site condition/field inspection during excavation.

Slope indicators must be installed during the shoring work.

Schematic drawing for the proposed permanent drainage system is enclosed (Drawing No. 2).

**In addition, a pre-construction survey of the surrounding structures/roads is recommended prior to commencement of shoring construction. The shoring system and surrounding structures must be monitored for horizontal and vertical movements, prior to, during and after the excavation.**

## 11.0 SLAB ON GRADE AND PERMANENT DRAINAGE

The City of Toronto – Toronto Water requires that any private water to be discharged into the City sewer system must have a permit or agreement in place in order to discharge; this applies to all water not purchased from the City water supply. For temporary dewatering during the construction phase, this includes all groundwater and storm water that is collected or encountered during site excavation.

For Private Water Discharge System (PWDS) this includes all groundwater that is constantly pumped as a result of the PWDS elevation located below the groundwater table elevation, or through storm water infiltration.

Toronto Water has indicated that PWDS systems may only be permitted through recirculation via an infiltration gallery and discharge to sewers may be prohibited. Otherwise, a fully waterproofed substructure may be required in the event that infiltration is not feasible. The Client must obtain permission and confirm discharge approval from Toronto Water directly (see Appendix C).

**Should the PWDS/infiltration gallery alternative be adopted and approved by the City,** the lowest garage/basement floor slab can be constructed as slab on grade (SOG), supported by competent native undisturbed silt/silty clay/sandy silt soils and/or engineered fill.

Upon completion of foundation work, the SOG should rest on a well compacted bed of size 19 mm clear stone at least 200 mm thick. The stone bed would act as a barrier and prevent capillary rise of moisture from the subgrade to the floor slab.

A permanent Private Water Drainage System (PWDS), as shown on Drawings No. 2 and 3, where shoring is constructed, should be considered.

To minimize siltation, all drainage pipe connections must be solid slotted PVC, with elbows and Ts, no “butt” end connections should be permitted. The pipes should slope to a sump at a minimum 1% slope.

Perimeter drainage pipes, with a positive gravity outlet, should be solid and slotted PVC with a minimum of 0.5% slope. In addition, silt traps must be provided at

convenient/accessible locations.

We request that PWDS drawings indicate design elevations for both perimeter and underfloor installation. MCR will provide calculations for sizing of permanent pumps, when required.

Upon completion of general excavation, scope and adequacy of the PWDS is to be re-evaluated. The installation of PWDS must be inspected by our office, prior to placement of filter stone.

Any design changes must be approved by the architect and reflected on mandatory as built drawings.\*

\* A copy of this page "Slab on grade and Permanent Water Drainage System" page should be posted at a site office as a permanent display.

In addition, the elevator pits should be fully waterproofed as shown on Drawing No. 4.

## 12.0 PAVEMENT

The critical section of pavement will be at the transition from the infinitely rigid substructure onto soil/backfill subgrade.

As a result, we suggest that an approach type slab be constructed at the entrance/exit points, as shown on Drawing No. 5.

The approach slab will alleviate detrimental effects of dynamic loading/settlement/pavement depression in the backfill to the rigid substructure.

All granular materials used in the pavement construction should be compacted to 100% of the Standard Proctor Maximum Dry Density.

Asphaltic concrete layer should be compacted to the range of 92 to 96.5% of maximum relative density.



Typical flexible pavement designs are as follows:

Pavement Layer	Recommended Thickness for Light Duty Parking	Recommended Thickness for Heavy Duty Parking
Asphaltic Concrete	40 mm OPSS HL 3 40 mm OPSS HL 8	50 mm OPSS HL 3 75 mm OPSS HL 8
OPSS Granular A Base (or 20mm Crushed Limestone)	150 mm	150 mm
OPSS Granular B	200 mm	350 mm

Upper 300 mm of the subgrade should be compacted to 98% SPMDD.

Implementation of a rigid pavement structure is suggested for areas with intense truck use, parking and turning vehicles. The minimum recommendation for rigid pavement structure is presented in following table.

Pavement Layer	Compaction Requirements	Heavy Duty Pavement
Portland Cement Concrete (CAN3-CSA A23.1) - Class C-2	CAN3-CSA A23.1	225 mm
Base Course: Granular A (OPSS 1010) or 19 mm Crusher Run Limestone	100% Standard Proctor Maximum Dry Density (ASTM-D698)	150 mm

A typical pavement structure above garage roof slab, please see Drawings No. 6 and 7.

### 13.0 METHANE GAS

The methane gas concentrations, presented on the attached borehole log sheets, are below the maximum MOE allowable limit of 5.0 % of Lower Explosive Limit (L.E.L.).

## 14.0 GENERAL COMMENTS

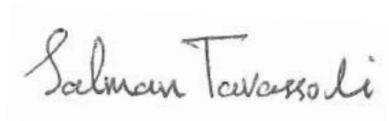
The comments given in this report are intended only as guidance for design engineers and are subject to field verification during construction. As more specific subsurface information, with respect to conditions between boreholes becomes available during excavations on the subject site, this report should be updated.

Contractors bidding on or undertaking the work should decide on their own investigations, as well as their own interpretations of the factual borehole results. This concern specifically applies to the classification of the subsurface soil and the potential reuse of these soils on/off site.

The contractors must draw their own conclusions as to how the near surface and subsurface conditions may affect them.

We trust this report contains information requested at this time. However, if any clarification is required or if we can be of further assistance, please call us.

Respectfully,  
McCLYMONT & RAK ENGINEERS INC.

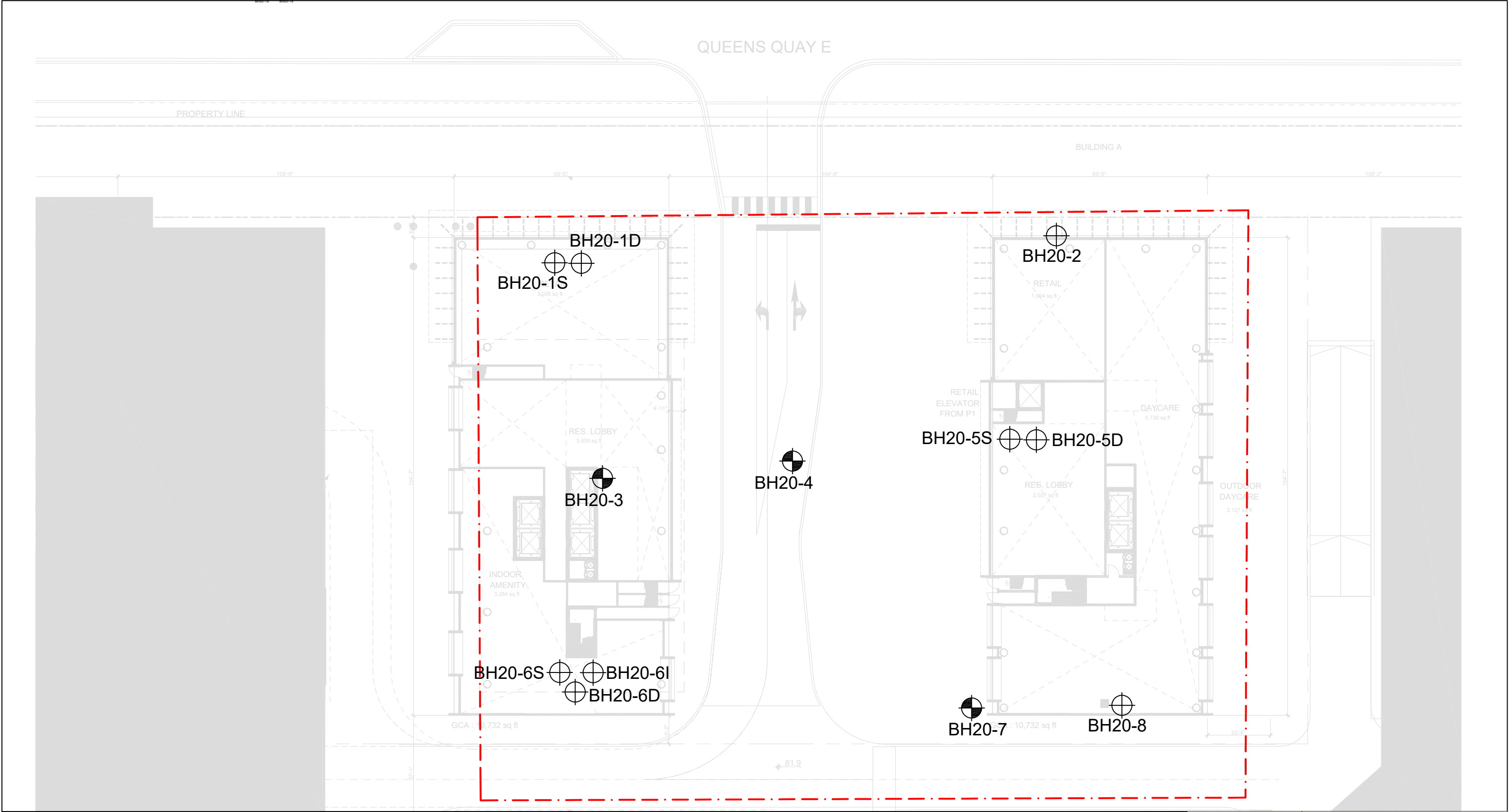


S. Tavassoli, E.I.T.



L.J. Rak, M.Eng., P.Eng.

# **DRAWINGS**



**LEGEND:**

- PHASE ONE PROPERTY BOUNDARY
- BOREHOLE/MONITORING WELL INSTALLED BY MCR, 2020

PROJECT NORTH

TRUE NORTH

0 5 10 20

SCALE (m)

**MCR**

**McCLYMONT & RAK**  
ENGINEERS, INC.  
GEO-ENVIRONMENTAL CONSULTANTS

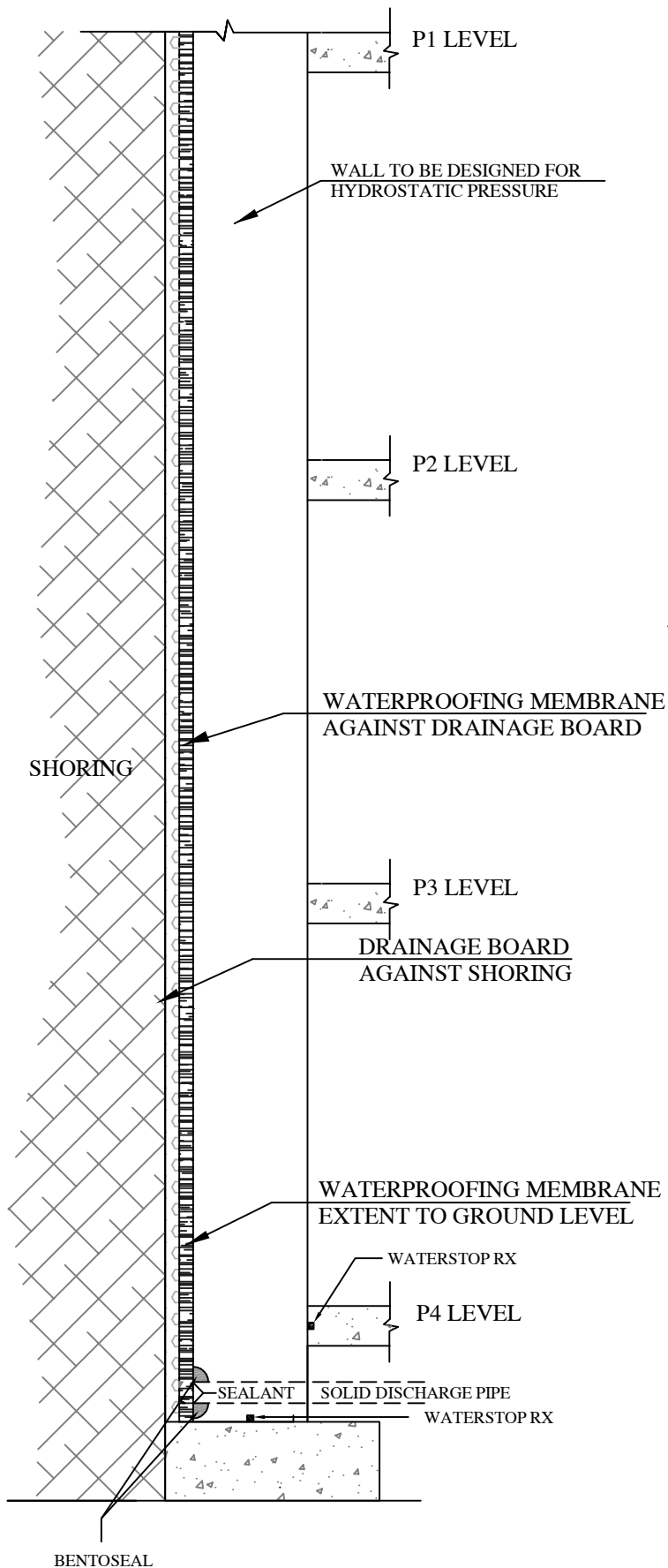
PIER 27, YONGE STREET & QUEENS QUAY EAST, TORONTO, ONTARIO

**BOREHOLE LOCATION PLAN**

Project No. G4842	Date OCTOBER 2020	Drawing No. 1
----------------------	----------------------	------------------

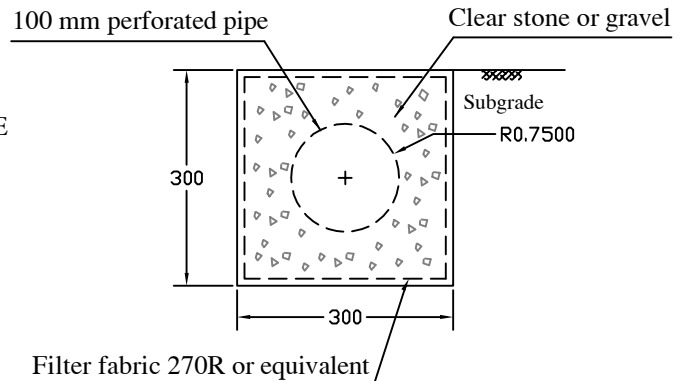
Drawing Notes: Image drafted from property survey, Toronto Maps, Google Maps, and site inspections. Not for construction purposes.

## SUGGESTED EXTERIOR DRAINAGE AGAINST SHORING



### NOTE:

- \* All permanent drainage pipes must have Geotextile filter sleeve to prevent long term silting. To further minimize siltation of the drainage system, all drainage pipe connections must be solid PVC elbows and Ts, no "butt" end connections should be permitted.
- \* Perimeter collection pipe to be solid pipe.



DETAILS OF SUB-FLOOR DRAINS  
TO BE PLACED IN PARALLEL ROWS 6- 8M (20'- 25')  
CENTERLINE TO CENTERLINE.

**McClymont and Rak Engineers Inc.**  
**GEO-ENVIRONMENTAL CONSULTANTS**  
1271 DENISON STREET, UNIT 45, MARKHAM, ON. TEL: 905 470 0160 FAX: 905 475 6371

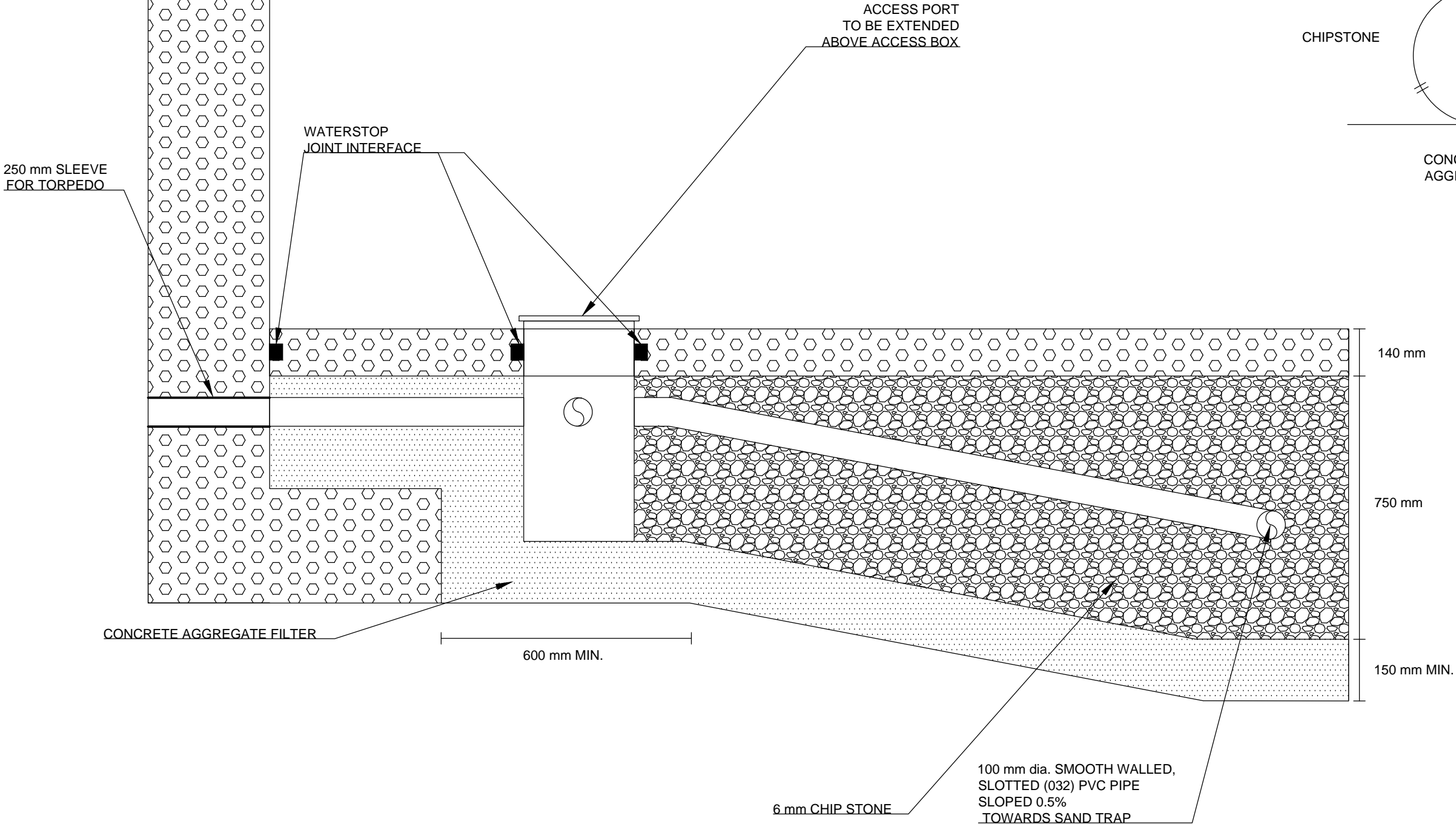
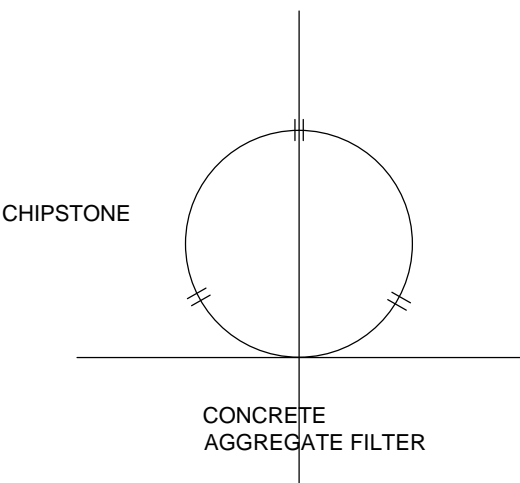
Project : PROPOSED DEVELOPMENT

Scale : N.T.S.

Date :

Drawing No.  
2

CROSS SECTION:  
100 mm dia.  
SMOOTH PVC PIPE

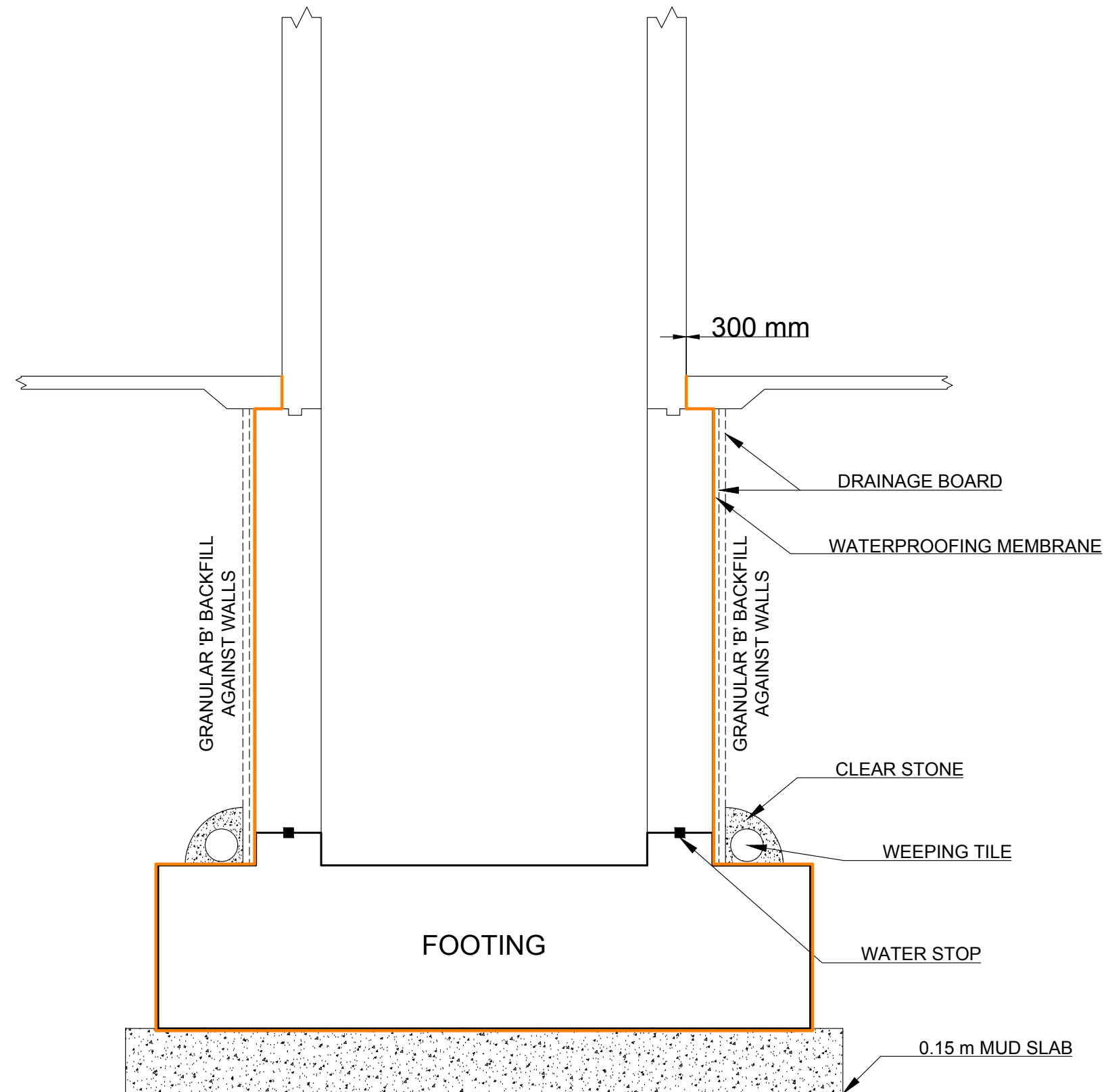


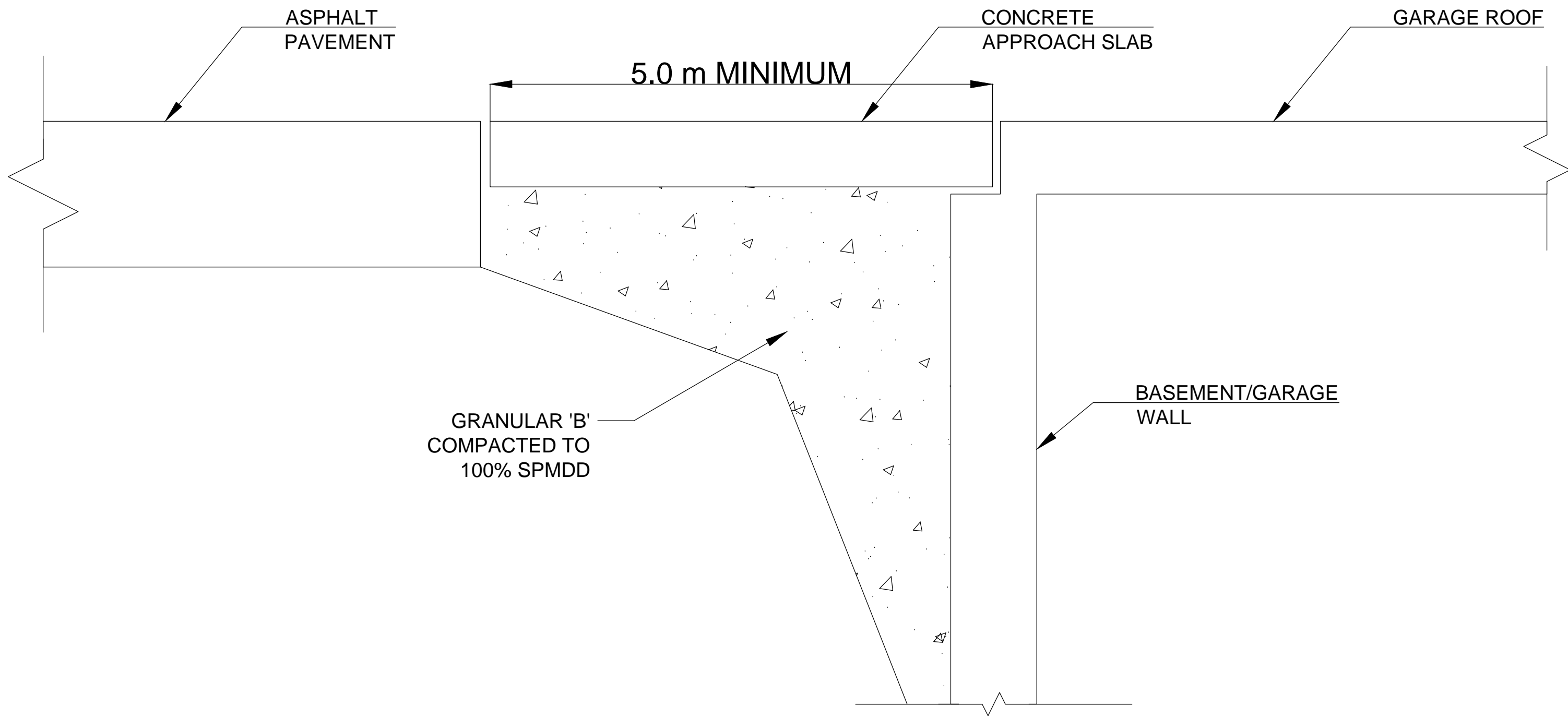
McCLYMONT & RAK  
ENGINEERS, INC.  
GEO-ENVIRONMENTAL CONSULTANTS


PRIVATE WATER  
DRAINAGE SYSTEM

Scale: NTS

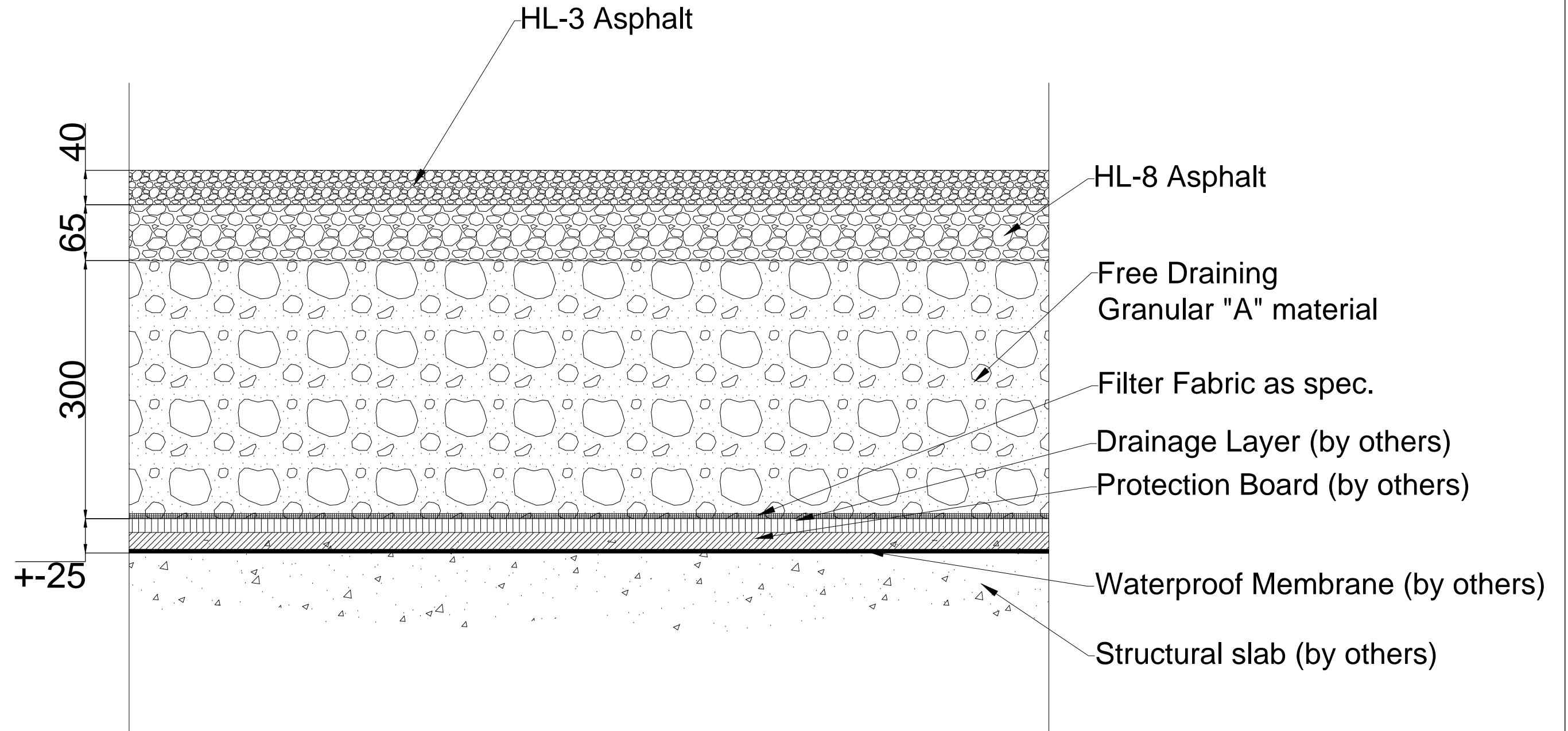
Drawing No. 3

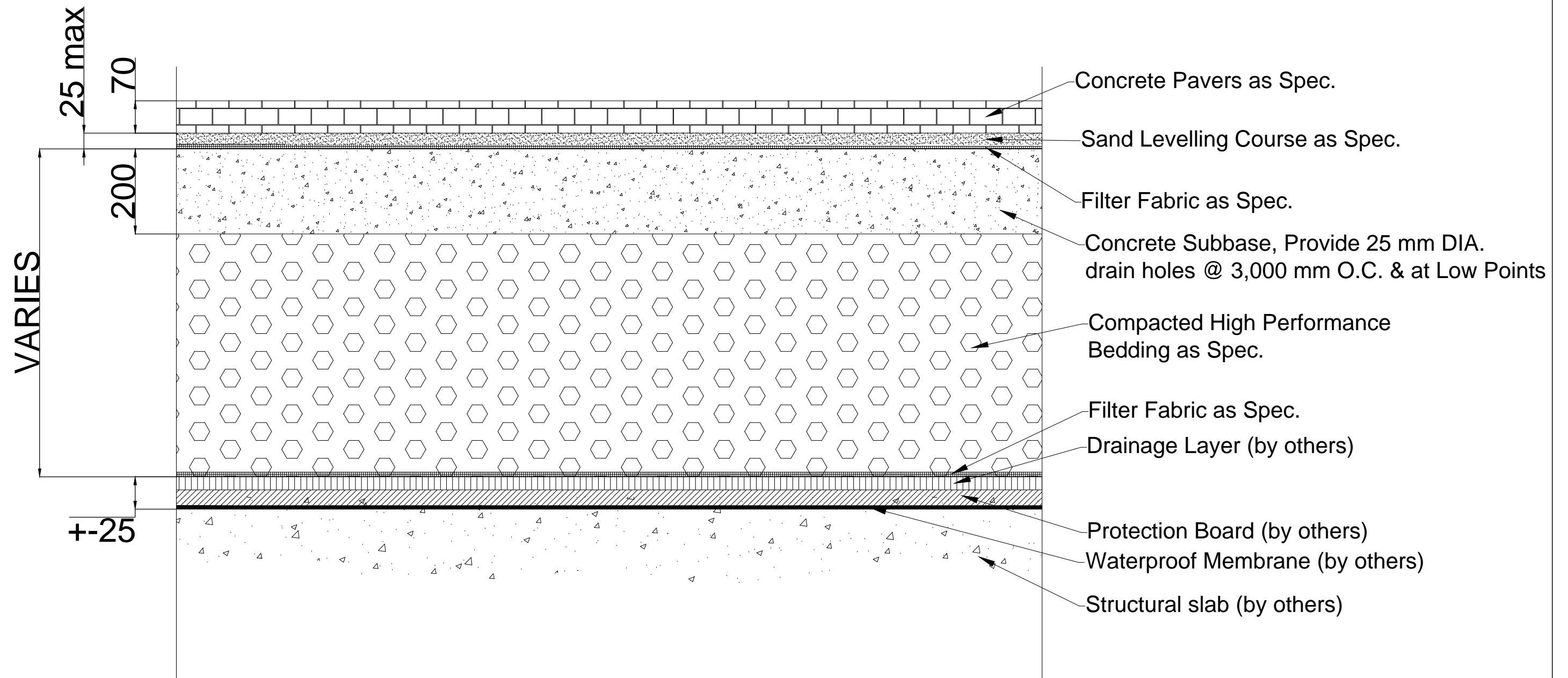




 <b>McCLYMONT &amp; RAK</b> ENGINEERS, INC. GEO-ENVIRONMENTAL CONSULTANTS	
SUGGESTED APPROACH SLAB DETAIL	
Scale: NTS	Drawing No. 5







## **APPENDIX A**

Green Roof Statistics

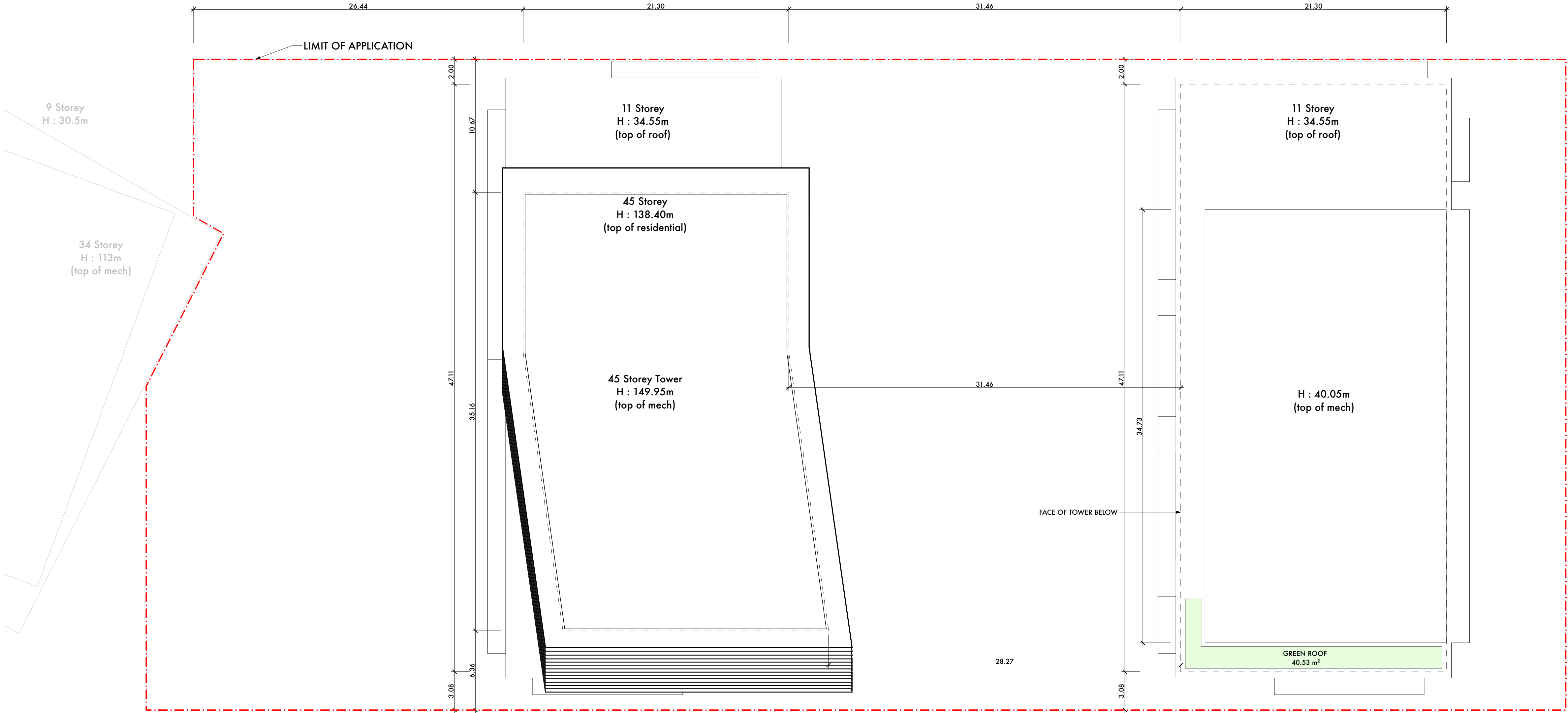
Toronto Green Standard Version 3.0

BUILDING F		Proposed
Gross Floor Area, as defined in Green Roof Bylaw (m <sup>2</sup> )		34348 m2
Total Roof Area (m <sup>2</sup> )		1145 m2
Area of Residential Private Terraces (m <sup>2</sup> )		0 m2
Rooftop Outdoor Amenity Space, if in a Residential Building (m <sup>2</sup> )		395 m2
Area of Renewable Energy Devices (m <sup>2</sup> )		0 m2
Tower (s)Roof Area with floor plate less than 750 m <sup>2</sup>		750 m2
Total Available Roof Space (m <sup>2</sup> )		0 m2
Green Roof Coverage		Required
Coverage of Available Roof Space (m <sup>2</sup> )		0
Coverage of Available Roof Space (%)		

BUILDING A		Proposed
Gross Floor Area, as defined in Green Roof Bylaw (m <sup>2</sup> )		10397 m2
Total Roof Area (m <sup>2</sup> )		1002 m2
Area of Residential Private Terraces (m <sup>2</sup> )		0 m2
Rooftop Outdoor Amenity Space, if in a Residential Building (m <sup>2</sup> )		260 m2
Area of Renewable Energy Devices (m <sup>2</sup> )		0 m2
Tower (s)Roof Area with floor plate less than 750 m <sup>2</sup>		674 m2
Total Available Roof Space (m <sup>2</sup> )		67.55 m2
Green Roof Coverage		Required
Coverage of Available Roof Space (m <sup>2</sup> )		40.53 m2
Coverage of Available Roof Space (%)		60%

BUILDING F

BUILDING A



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2. These Contract Documents are the property of the Architect. The Architect bears no responsibility for the interpretation of these documents by the Contractor. Upon written application, the Architect will provide written/graphic clarification or supplementary information regarding the intent of the Contract Documents. The Architect will review Shop Drawings submitted by the Contractor for design conformance only.

3. Drawings are not to be scaled for construction. The Contractor is to verify all existing conditions and dimensions required to perform the work and report any discrepancies with the Contract Documents to the Architect before commencing any work.

4. Positions of exposed finished mechanical or electrical devices, fittings, and fixtures are indicated on architectural drawings. The locations shown on the architectural drawings govern over the Mechanical and Electrical drawings. Those items not clearly located will be located as directed by the Architect.

5. These drawings are not to be used for construction unless noted below as "Issuance: For Construction"

6. All work is to be carried out in conformance with the Code and Bylaws of the authorities having jurisdiction.

7. The Architect of these plans and specifications gives no warranty or representation to any party about the constructability of the building(s) represented by them. All contractors or subcontractors must satisfy themselves when bidding and at all times ensure that they can properly construct the work represented by these plans.

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NO	ISSUANCE	DATE
1	SPA/OPA/ZBA	-
2	-	-
3	-	-
4	-	-
5	-	-

aA

architectsAlliance

205 - 317 Adelaide Street West  
Toronto, ON M5V 1P9 Canada  
t 416 593 6500  
f 416 593 4911  
info@architectsalliance.com  
www.architectsalliance.com

Pier 27 Phase 3  
(buildings F and A)  
25&35 Queens Quay East

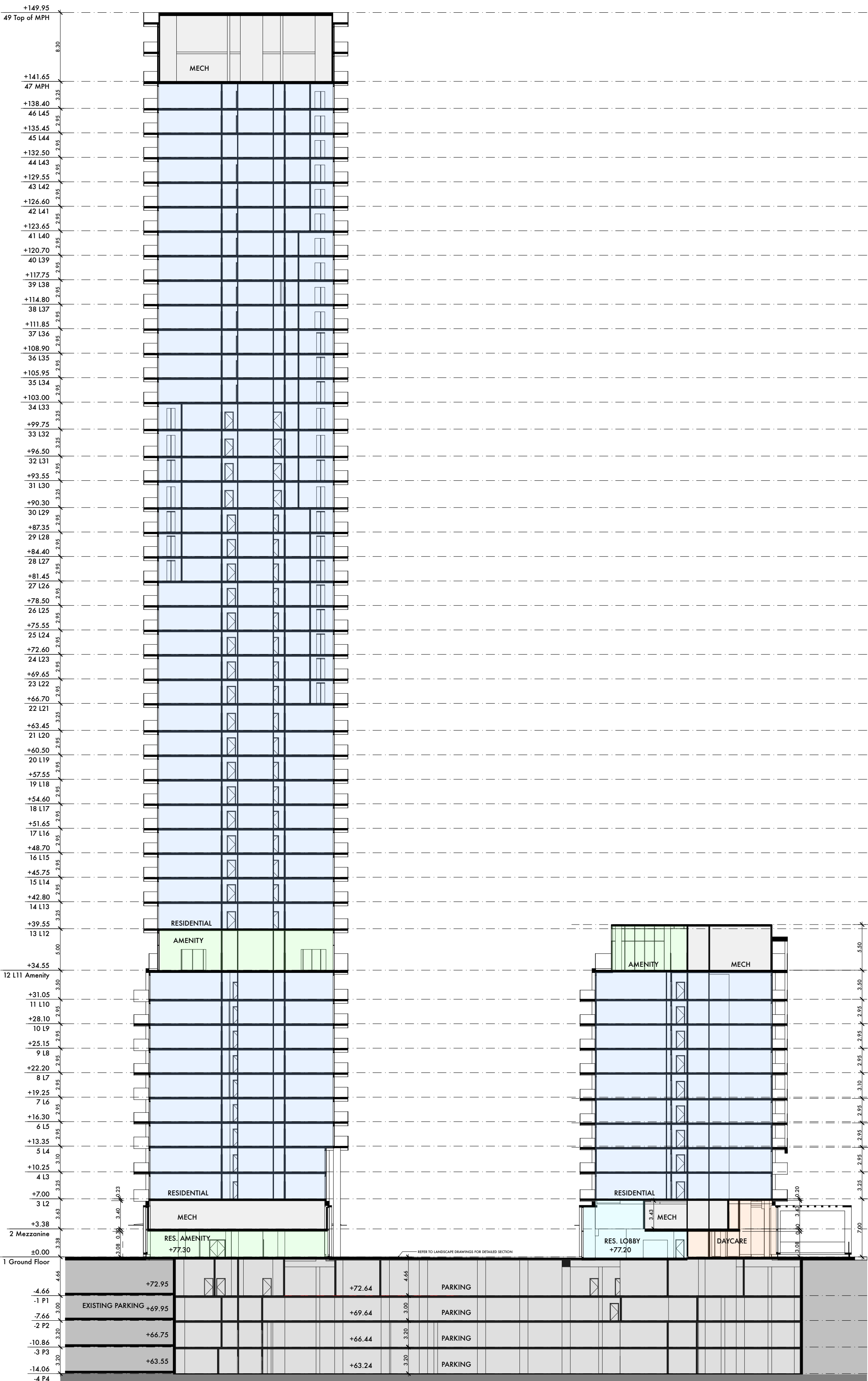
Pier 27 Toronto (Northeast) Inc.  
56 The Esplanade, suite 308  
Toronto M5E 1A7

Roof Plan

Project No.

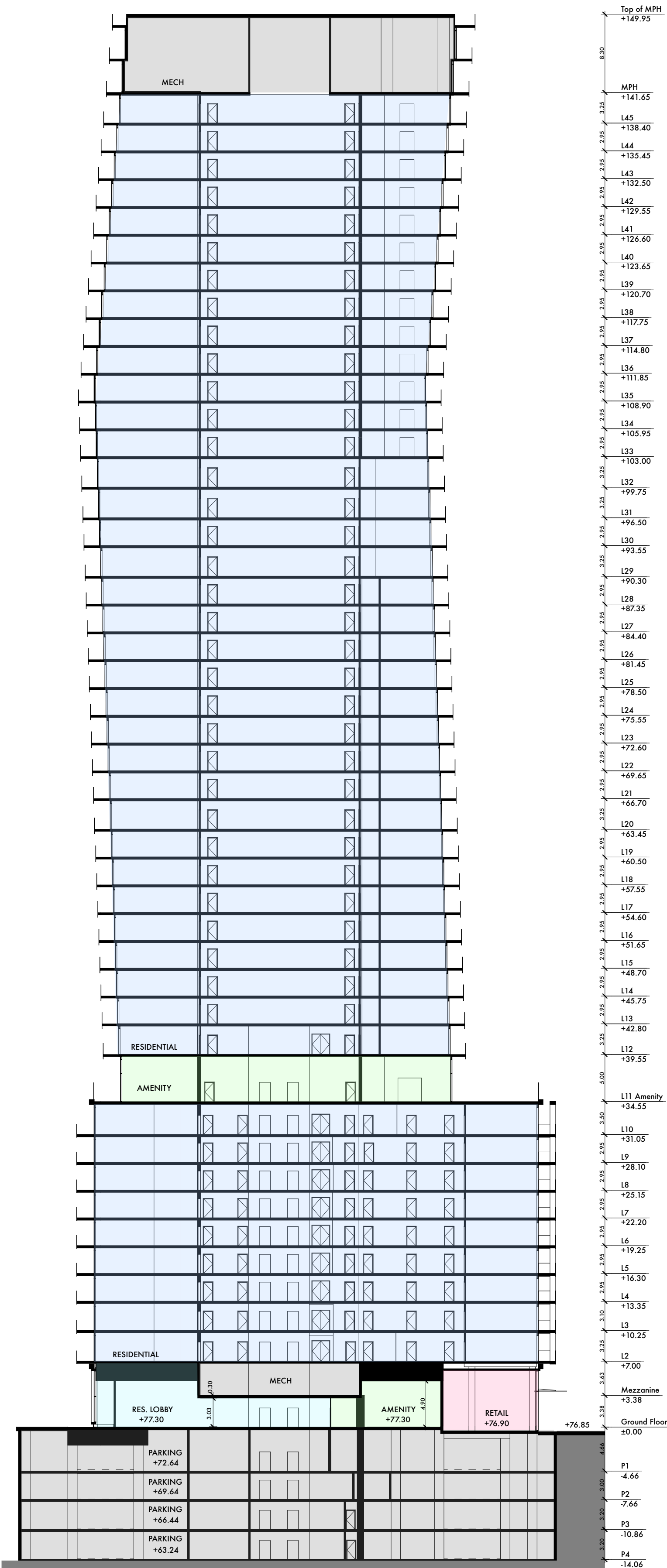
1:200

A.1.21



BUILDING F

BUILDING A



BUILDING F

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2. These Contract Documents are the property of the Architect. The Architect bears no responsibility for the interpretation of these documents by the Contractor. Upon written application, the Architect will provide written/graphic clarification or supplementary information regarding the intent of the Contract Documents. The Architect will review Shop Drawings submitted by the Contractor for design conformance only.

3. Drawings are not to be scaled for construction. The Contractor is to verify all existing conditions and dimensions required to perform the work and report any discrepancies with the Contract Documents to the Architect before commencing any work.

4. Positions of exposed finished mechanical or electrical devices, fittings, and fixtures are indicated on architectural drawings. The locations shown on the architectural drawings govern over the Mechanical and Electrical drawings. Those items not clearly located will be located as directed by the Architect.

5. These drawings are not to be used for construction unless noted below as "Issuance: For Construction"

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7. The Architect of these plans and specifications gives no warranty or representation to any party about the constructability of the building(s) represented by them. All contractors or subcontractors must satisfy themselves when bidding and at all times ensure that they can properly construct the work represented by these plans.

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NO	ISSUANCE	DATE
1	SPA/OPA/ZBA	-
2	-	-
3	-	-
4	-	-
5	-	-

aA

architectsAlliance

205 - 317 Adelaide Street West  
Toronto, ON M5V 1P9 Canada  
t 416 593 6500  
f 416 593 4911  
info@architectsalliance.com  
www.architectsalliance.com

## Pier 27 Phase 3 (buildings F and A) 25&35 Queens Quay East

Pier 27 Toronto (Northeast) Inc.  
56 The Esplanade, suite 308  
Toronto M5E 1A7

Section

Project No.

1:350

A.3.1

## **APPENDIX B**

# RECORD OF BOREHOLE 20-1-S

PROJECT : MG4842  
LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
STARTED : September 21, 2020  
COMPLETED : September 21, 2020


**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
DATUM Geodetic

[illegible]

## GROUNDWATER ELEVATIONS

▽ SHALLOW/SINGLE INSTALLATION  
WATER LEVEL: 2.55 m bgs

 DEEP/DUAL INSTALLATION  
WATER LEVEL:

LOGGED : PL  
CHECKED : NS



















# RECORD OF BOREHOLE 20-1-D


PROJECT : MG4842  
 LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
 STARTED : September 21, 2020  
 COMPLETED : September 21, 2020


**MC CLYMONT & RAK  
 ENGINEERS, INC.**

SHEET 1 OF 1  
 DATUM Geodetic

DEPTH SCALE (metres)	BORING METHOD	SOIL PROFILE		SAMPLES		ORGANIC VAPOUR READINGS (ppm)				SHEAR STRENGTH: Cu, KPa				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	nat V -  rem V -  Q -  U - 				WATER CONTENT, PERCENT					
								% LEL - (hexane) 				wp  w  wl 					
		GROUND SURFACE		76.93				100	200	300	400	20	40	60	80		
2	POWER BORING HOLLOW STEM AUGER	FILL: sand and silt, trace clay and organics, brown, moist, loose to compact        - decayed wood at 2.44 m depth			1	SS	15	0									Flush Mount Cover  Bentonite  1.52 m Long 50 mm ID PVC Riser
					2	SS	10	40									
					3	SS	3	50									
					4	SS	25	30									
					5	SS	7	40									
4		SAND: medium to fine, dark brown to black, wet, loose			6	SS	9	75									
6		SILT: some fine sand, dark brown to black, wet, soft			7	SS	4	35									
8		SILTY CLAY: trace sand, gravel and shells, black to grey, moist, soft to hard			8	SS	3	130									
10					9	SS	3	140									67.18
12		WEATHERED SHALE: grey, moist			10	SS	4	60									66.26
14		End of Borehole.  Note: 1) Borehole remained dry on completion of drilling. 2) Water level was measured at 11.29 m depth on September 28, 2020			11	SS	>100	0									3.05 m Long 50 mm ID Well Screen  64.13

## GROUNDWATER ELEVATIONS

 SHALLOW/SINGLE INSTALLATION  
 WATER LEVEL: 7.46 m bgs

 DEEP/DUAL INSTALLATION  
 WATER LEVEL:

LOGGED : PL  
 CHECKED : NS














MCR LOG ENVIRONMENTAL 4842.GPJ 10/14/20

# RECORD OF BOREHOLE 20-3

PROJECT : MG4842  
 LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
 STARTED : September 22, 2020  
 COMPLETED : September 22, 2020

**MC CLYMONT & RAK  
 ENGINEERS, INC.**

SHEET 1 OF 1  
 DATUM Geodetic

DEPTH SCALE (metres)	BORING METHOD	SOIL PROFILE			SAMPLES		ORGANIC VAPOUR READINGS (ppm)				SHEAR STRENGTH: Cu, KPa				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION	
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	nat V -  rem V -  U - 				nat V -  rem V -  U - 					
								100 200 300 400				20 40 60 80					
								% LEL - (hexane) 				WATER CONTENT, PERCENT					
								wp  w  wl 									
								10 20 30 40									
		GROUND SURFACE		76.88													
	POWER BORING HOLLOW STEM AUGER	FILL: sand and gravel, brown, moist, compact to loose			1	SS	26	5									
		FILL: clay and silt, some organics, trace of sand and gravel, dark brown to black, moist, loose			2	SS	6	10									

## GROUNDWATER ELEVATIONS

▽ SHALLOW/SINGLE INSTALLATION  
 WATER LEVEL: m bgs

▼ DEEP/DUAL INSTALLATION  
 WATER LEVEL: m bgs

LOGGED : PL  
 CHECKED : NS

# RECORD OF BOREHOLE 20-4


PROJECT : MG4842  
LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
STARTED : September 24, 2020  
COMPLETED : September 24, 2020


**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
DATUM Geodetic

[illegible]

## GROUNDWATER ELEVATIONS

 SHALLOW/SINGLE INSTALLATION  
WATER LEVEL: m bgs

 DEEP/DUAL INSTALLATION  
WATER LEVEL:

LOGGED : PL  
CHECKED : NS

MCR LOG ENVIRONMENTAL 4842.GPJ 10/14/20

# RECORD OF BOREHOLE 20-5-D

PROJECT : MG4842  
LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
STARTED : September 23, 2020  
COMPLETED : September 23, 2020


**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
DATUM Geodetic

[illegible]

## GROUNDWATER ELEVATIONS

▽ SHALLOW/SINGLE INSTALLATION  
WATER LEVEL: 11.29 m bgs

 DEEP/DUAL INSTALLATION  
WATER LEVEL:

LOGGED : PL  
CHECKED : NS







MCR LOG ENVIRONMENTAL 4842.GPJ 10/14/20

# RECORD OF BOREHOLE 20-6-S


PROJECT : MG4842  
 LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
 STARTED : September 22, 2020  
 COMPLETED : September 22, 2020


**MC CLYMONT & RAK  
 ENGINEERS, INC.**

SHEET 1 OF 1  
 DATUM Geodetic

DEPTH SCALE (metres)	BORING METHOD	SOIL PROFILE		SAMPLES		ORGANIC VAPOUR READINGS (ppm)				SHEAR STRENGTH: Cu, KPa				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	nat V - 				Q - 					
								rem V - 				U - 					
								% LEL - (hexane) 				WATER CONTENT, PERCENT					
								wp  w									
								10 20 30 40									
		GROUND SURFACE		77.06													
		STRAIGHT DRILLING TO 9.14 m DEPTH															
2	POWER BORING HOLLOW STEM AUGER																
4																	
6																	
8																	
10																	
		End of Borehole.		67.92 9.14													
		Note: 1) Borehole remained dry on completion of drilling. 2) Water level was measured at 2.66 m depth on September 28, 2020															

## GROUNDWATER ELEVATIONS

 SHALLOW/SINGLE INSTALLATION  
 WATER LEVEL: 2.66 m bgs

 DEEP/DUAL INSTALLATION  
 WATER LEVEL:

LOGGED : PL  
 CHECKED : NS

# RECORD OF BOREHOLE 20-6-I

PROJECT : MG4842  
LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
STARTED : September 24, 2020  
COMPLETED : September 24, 2020

**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
DATUM Geodetic

[illegible]

## GROUNDWATER ELEVATIONS

▽ SHALLOW/SINGLE INSTALLATION  
WATER LEVEL: 2.84 m bgs

 DEEP/DUAL INSTALLATION  
WATER LEVEL:

LOGGED : PL  
CHECKED : NS

# RECORD OF BOREHOLE 20-6-D

PROJECT : MG4842  
LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
STARTED : September 22, 2020  
COMPLETED : September 22, 2020


**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
DATUM Geodetic

[illegible]

## GROUNDWATER ELEVATIONS

▽ SHALLOW/SINGLE INSTALLATION  
WATER LEVEL: 9.80 m bqs

 DEEP/DUAL INSTALLATION  
WATER LEVEL:

LOGGED : PL  
CHECKED : NS

MCR LOG ENVIRONMENTAL 4842.GPJ 10/14/20













MCR LOG ENVIRONMENTAL 4842.GPJ 10/14/20

# RECORD OF BOREHOLE 20-8


PROJECT : MG4842  
 LOCATION : Pier 27, Yonge Street & Queens Quay East, Toronto, Ontario  
 STARTED : September 24, 2020  
 COMPLETED : September 24, 2020


**MC CLYMONT & RAK  
ENGINEERS, INC.**

SHEET 1 OF 1  
 DATUM Geodetic

DEPTH SCALE (metres)	BORING METHOD	SOIL PROFILE		SAMPLES		ORGANIC VAPOUR READINGS (ppm)				SHEAR STRENGTH: Cu, KPa				ADDITIONAL LAB. TESTING	PIEZOMETER OR STANDPIPE INSTALLATION		
		DESCRIPTION	STRATA PLOT	ELEV. DEPTH (m)	NUMBER	TYPE	BLOWS/0.3m	nat V -  rem V -  U - 				Q -  U - 					
								100 200 300 400				20 40 60 80					
								% LEL - (hexane) 				WATER CONTENT, PERCENT					
								wp  w 									
								20 40 60 80				10 20 30 40					
		GROUND SURFACE		77.05													
		75 mm CONCRETE		76.97 0.08											Flush Mount Cover		
		525 mm GRANULAR FILL: sand and gravel, trace of organics, brown, moist, compact.			1	SS	23	0									
		FILL: clayey silt with organics, trace of sand and gravel, trace of clinkers and brick pieces, black, moist, compact.		76.44 0.61											Bentonite		
					2	SS	13	0							1.52 m Long 50 mm ID PVC Riser		
					3	SS	7	0							75.53 Silica Sand		
					4	SS	5	0									
					5	SS	3	0							3.05 m Long 50 mm ID Well Screen		

## GROUNDWATER ELEVATIONS

 SHALLOW/SINGLE INSTALLATION  
 WATER LEVEL: 2.25 m bgs

 DEEP/DUAL INSTALLATION  
 WATER LEVEL:

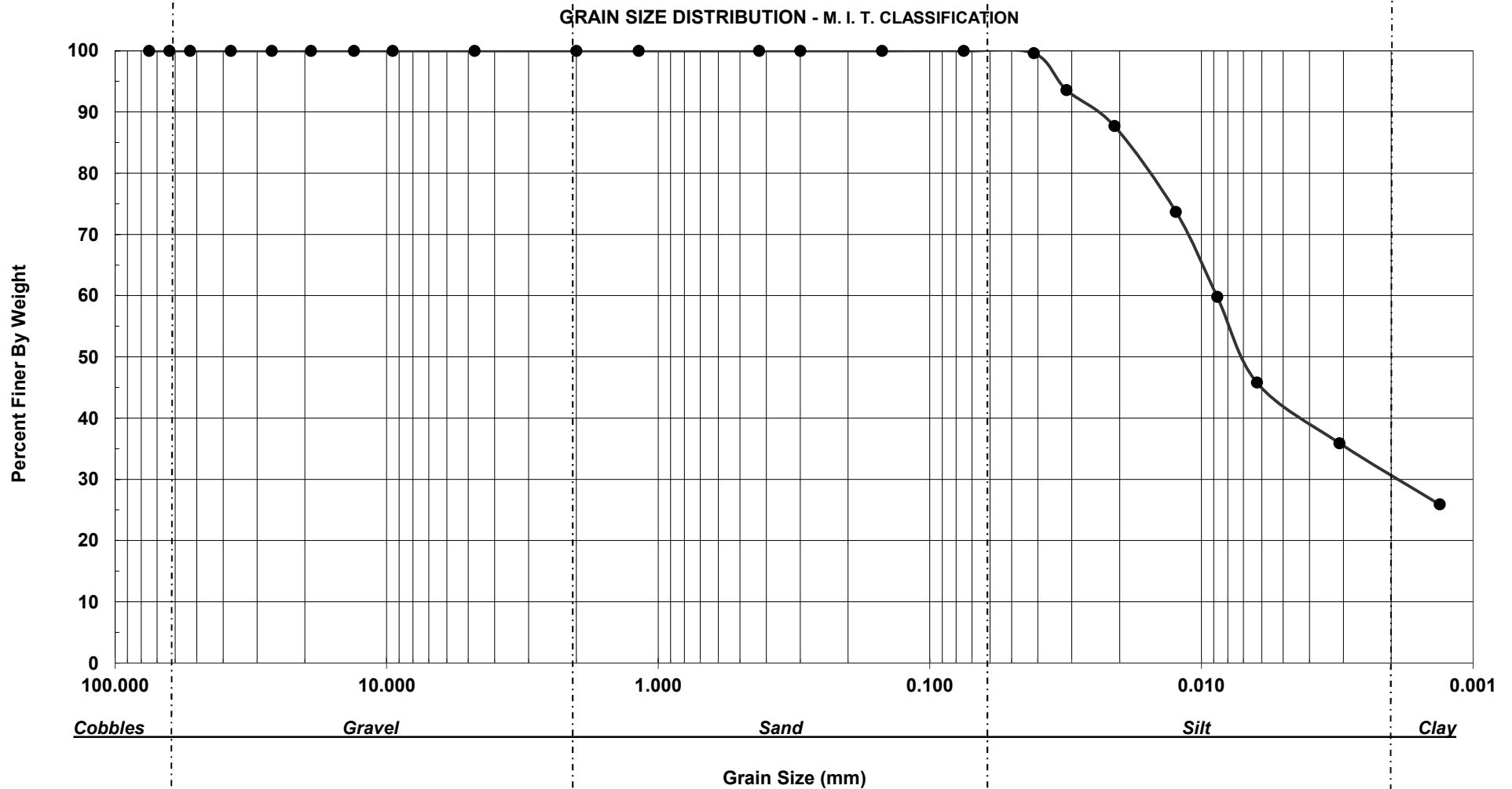
LOGGED : PL  
 CHECKED : NS

**McCLYMONT AND RAK ENGINEERS INC.**  
**GEO-ENVIRONMENTAL CONSULTANTS**  
111 Zenway Blvd., Unit 4, Vaughan, Ontario L4H 3H9  
TEL: 416-675-0160 FAX: 905-851-1722

**GRAIN SIZE ANALYSIS (Gradation Curve)**

Job No.: **G 4842**  
Sample Location: **BH 20-5D**  
Sampled by:  
Tested by: **M.M.**

Report No.: **1**  
Sample No.: **SS 8**  
Date Sampled:  
Date Tested: **September, 2020**

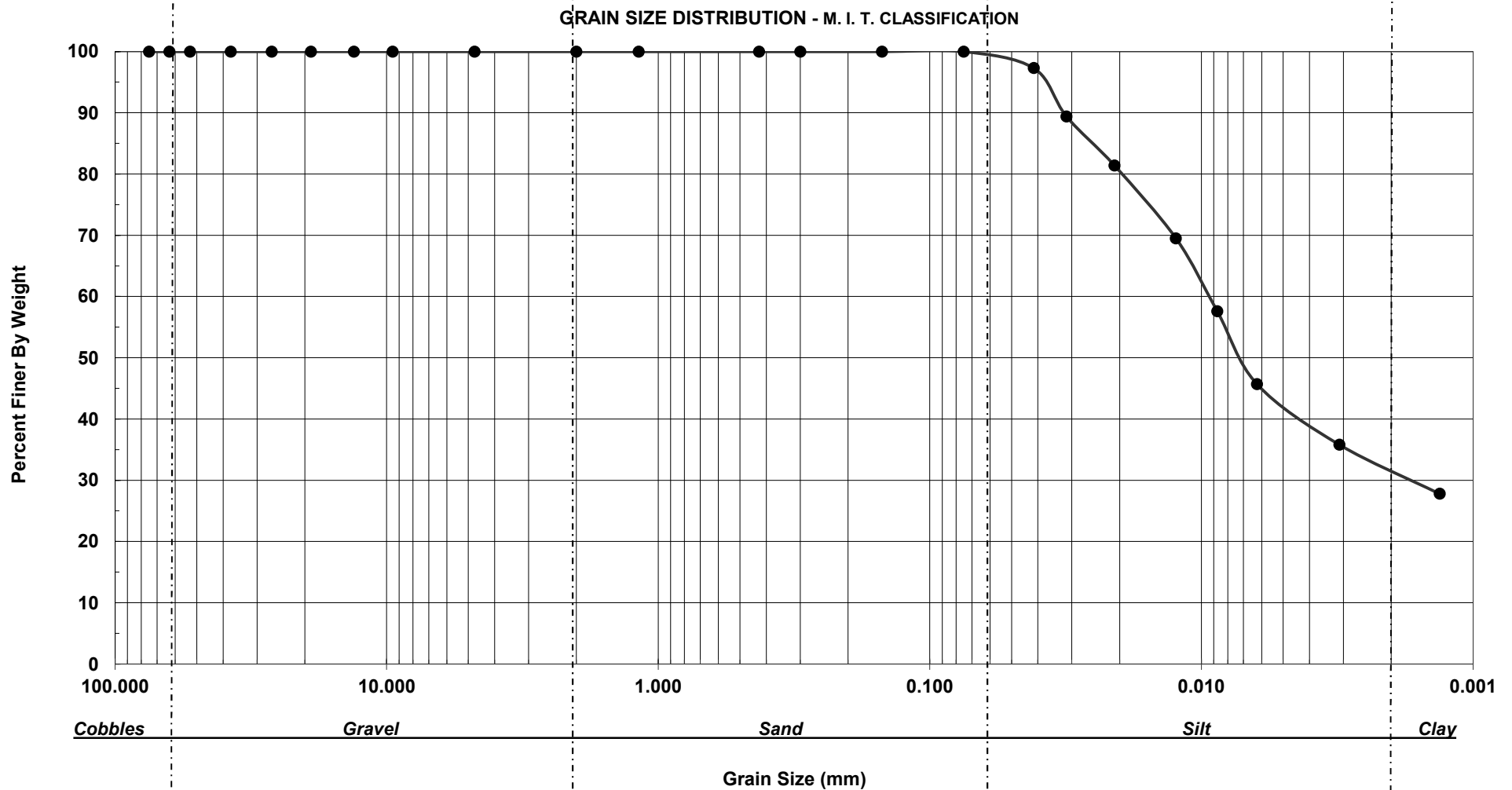


**McCLYMONT AND RAK ENGINEERS INC.**  
**GEO-ENVIRONMENTAL CONSULTANTS**  
111 Zenway Blvd., Unit 4, Vaughan, Ontario L4H 3H9  
TEL: 416-675-0160 FAX: 905-851-1722

**GRAIN SIZE ANALYSIS (Gradation Curve)**

Job No.: **G 4842**  
Sample Location: **BH 20-6D**  
Sampled by:  
Tested by: **M.M.**

Report No.: **2**  
Sample No.: **SS 10**  
Date Sampled:  
Date Tested: **September, 2020**



## **APPENDIX C**

[Company Letterhead]

[Company Name]

[Property Owner Name and Contact Information]

[Date DD/MMM/YYYY]

**Attention:** Executive Director, Engineering and Construction Services  
c/o Manager, Development Engineering

[ADDRESS]

**cc:** General Manager, Toronto Water  
c/o Manager, Environmental Monitoring and Protection Unit  
30 Dee Ave, Toronto ON M9N 1S9

Dear Sir or Madam,

I \_\_\_\_\_, confirm and undertake that I will maintain all building(s) on the subject lands (MUNICIPAL ADDRESS) in a manner which will not discharge, directly or indirectly, any private water collected from subsurface drainage system consisting of but not limited to weeping tile(s), foundation drain(s), private water collection sump(s), private water pump or any combination thereof for the disposal of private water to a private sewer connection directly or indirectly or drainage system for disposal directly or indirectly in a municipal sewer. All the water collected in the subdrainage collection system will be managed onsite all time via infiltration gallery/dry well. There will be no direct or indirect discharge of private water to City's sewer.

I am aware of MOECC and OBC requirements regarding infiltration gallery/dry well.

\_\_\_\_\_  
Name (printed) and Title

\_\_\_\_\_  
Email

\_\_\_\_\_  
Signature

I, [PRINT NAME], have the authority to bind the corporation.

[Company Letterhead]

[Company Name]

[Property Owner Name and Contact Information]

[Date DD/MMM/YYYY]

**Attention:** Executive Director, Engineering and Construction Services  
c/o Manager, Development Engineering

[ADDRESS]

**cc:** General Manager, Toronto Water  
c/o Manager, Environmental Monitoring and Protection Unit  
30 Dee Ave, Toronto ON M9N 1S9

Dear Sir or Madam,

I \_\_\_\_\_, confirm and undertake that I will construct and maintain all building(s) on the subject lands (MUNICIPAL ADDRESS) in a manner which shall be completely water-tight below grade and resistant to hydrostatic pressure without any necessity for Private Water Drainage System (subsurface drainage system) consisting of but not limited to weeping tile(s), foundation drain(s), private water collection sump(s), private water pump or any combination thereof for the disposal of private water on the surface of the ground or to a private sewer connection directly or indirectly or drainage system for disposal directly or indirectly in a municipal sewer.

\_\_\_\_\_  
Name (printed) and Title

\_\_\_\_\_  
Email

\_\_\_\_\_  
Signature

I, [PRINT NAME], have the authority to bind the corporation.

## **APPENDIX D**





Your Project #: 4842  
Your C.O.C. #: 152751

**Attention: Salman Tavassoli**

McClymont & Rak Engineers Inc  
111 Zenway Blvd  
Unit 4  
Vaughan, ON  
CANADA L4H 3H9

**Report Date: 2020/10/07**  
Report #: R6361523  
Version: 1 - Final

**CERTIFICATE OF ANALYSIS**

**BV LABS JOB #: COP3558**

**Received: 2020/09/28, 16:30**

Sample Matrix: Soil  
# Samples Received: 1

Analyses	Quantity	Date	Date	Laboratory Method	Analytical Method
		Extracted	Analyzed		
Chloride (20:1 extract)	1	2020/09/30	2020/10/01	CAM SOP-00463	SM 23 4500-Cl E m
Conductivity	1	2020/10/01	2020/10/02	CAM SOP-00414	OMOE E3530 v1 m
Moisture (Subcontracted) (1, 3)	1	N/A	2020/10/06	AB SOP-00002	CCME PHC-CWS m
Sulphide in Soil (1)	1	N/A	2020/10/06	AB SOP-00080	EPA9030B/SM4500S2-DF
pH CaCl2 EXTRACT	1	2020/10/01	2020/10/01	CAM SOP-00413	EPA 9045 D m
Resistivity of Soil	1	2020/09/29	2020/10/02	CAM SOP-00414	SM 23 2510 m
Sulphate (20:1 Extract)	1	2020/09/30	2020/10/01	CAM SOP-00464	EPA 375.4 m
Redox Potential (2, 4)	1	N/A	N/A		

**Remarks:**

Bureau Veritas Laboratories are accredited to ISO/IEC 17025 for specific parameters on scopes of accreditation. Unless otherwise noted, procedures used by BV Labs are based upon recognized Provincial, Federal or US method compendia such as CCME, MELCC, EPA, APHA.

All work recorded herein has been done in accordance with procedures and practices ordinarily exercised by professionals in BV Labs profession using accepted testing methodologies, quality assurance and quality control procedures (except where otherwise agreed by the client and BV Labs in writing). All data is in statistical control and has met quality control and method performance criteria unless otherwise noted. All method blanks are reported; unless indicated otherwise, associated sample data are not blank corrected. Where applicable, unless otherwise noted, Measurement Uncertainty has not been accounted for when stating conformity to the referenced standard.

BV Labs liability is limited to the actual cost of the requested analyses, unless otherwise agreed in writing. There is no other warranty expressed or implied. BV Labs has been retained to provide analysis of samples provided by the Client using the testing methodology referenced in this report. Interpretation and use of test results are the sole responsibility of the Client and are not within the scope of services provided by BV Labs, unless otherwise agreed in writing. BV Labs is not responsible for the accuracy or any data impacts, that result from the information provided by the customer or their agent.

Solid sample results, except biota, are based on dry weight unless otherwise indicated. Organic analyses are not recovery corrected except for isotope dilution methods.

Results relate to samples tested. When sampling is not conducted by BV Labs, results relate to the supplied samples tested.

This Certificate shall not be reproduced except in full, without the written approval of the laboratory.

Reference Method suffix "m" indicates test methods incorporate validated modifications from specific reference methods to improve performance.

\* RPDs calculated using raw data. The rounding of final results may result in the apparent difference.

- (1) This test was performed by BVLabs Calgary via Mississauga
- (2) This test was performed by Sub from Campo to Env. Testing Canada (Eurofins)
- (3) Offsite analysis requires that subcontracted moisture be reported.



Your Project #: 4842  
Your C.O.C. #: 152751

**Attention: Salman Tavassoli**

McClymont & Rak Engineers Inc  
111 Zenway Blvd  
Unit 4  
Vaughan, ON  
CANADA L4H 3H9

**Report Date: 2020/10/07**  
Report #: R6361523  
Version: 1 - Final

**CERTIFICATE OF ANALYSIS**

**BV LABS JOB #: C0P3558**

**Received: 2020/09/28, 16:30**

(4) Oxidation-Reduction Potential (ORP) values are determined using a Ag/AgCl reference electrode.

**Encryption Key**

Please direct all questions regarding this Certificate of Analysis to your Project Manager.

Antonella Brasil, Senior Project Manager

Email: Antonella.Brasil@bvlabs.com

Phone# (905)817-5817

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BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports. For Service Group specific validation please refer to the Validation Signature Page.



BUREAU  
VERITAS

BV Labs Job #: COP3558  
Report Date: 2020/10/07

McClymont & Rak Engineers Inc  
Client Project #: 4842

### RESULTS OF ANALYSES OF SOIL

BV Labs ID		NTH506			NTH506	NTH506	NTH506		
Sampling Date		2020/09/23			2020/09/23	2020/09/23	2020/09/23		
COC Number		152751			152751	152751	152751		
	UNITS	BH20-5D SS10	RDL	QC Batch	BH20-5D SS10 Lab-Dup	BH20-5D SS10 Lab-Dup 2	BH20-5D SS10 Lab-Dup 3	RDL	QC Batch
<b>Calculated Parameters</b>									
Resistivity	ohm-cm	1700		6971545					
<b>Inorganics</b>									
Soluble (20:1) Chloride (Cl-)	ug/g	83	20	6974855					
Conductivity	umho/cm	580	2	6976739					
Available (CaCl2) pH	pH	7.20		6976515					
Soluble (20:1) Sulphate (SO4)	ug/g	<20	20	6974862					
Sulphide	mg/kg	2.4 (1)	0.5	6986221	13.5 (2)	1.0 (2)	7.9 (2)	0.5	6986221
<b>Physical Testing</b>									
Moisture-Subcontracted	%	30	0.30	6986220					
RDL = Reportable Detection Limit QC Batch = Quality Control Batch Lab-Dup = Laboratory Initiated Duplicate (1) Duplicate exceeds acceptance criteria due to sample non homogeneity. Reanalysis yields similar results. Sample extracted past method-specified hold time. Sample contained greater than 10% headspace at time of extraction. (2) Recovery or RPD for this parameter is outside control limits. The overall quality control for this analysis meets acceptability criteria.									



BV Labs Job #: COP3558  
Report Date: 2020/10/07

McClymont & Rak Engineers Inc  
Client Project #: 4842

## TEST SUMMARY

**BV Labs ID:** NTH506  
**Sample ID:** BH20-5D SS10  
**Matrix:** Soil

**Collected:** 2020/09/23  
**Shipped:**  
**Received:** 2020/09/28

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Chloride (20:1 extract)	KONE/EC	6974855	2020/09/30	2020/10/01	Deonarine Ramnarine
Conductivity	AT	6976739	2020/10/01	2020/10/02	Yogesh Patel
Moisture (Subcontracted)	BAL	6986220	N/A	2020/10/06	Margarita Aguilera
Sulphide in Soil	SPEC	6986221	N/A	2020/10/06	Sonya Radvan
pH CaCl2 EXTRACT	AT	6976515	2020/10/01	2020/10/01	Surinder Rai
Resistivity of Soil		6971545	2020/10/02	2020/10/02	Automated Statchk
Sulphate (20:1 Extract)	KONE/EC	6974862	2020/09/30	2020/10/01	Deonarine Ramnarine
Redox Potential	COND	6988807	2020/10/07		Antonella Brasil

**BV Labs ID:** NTH506 Dup  
**Sample ID:** BH20-5D SS10  
**Matrix:** Soil

**Collected:** 2020/09/23  
**Shipped:**  
**Received:** 2020/09/28

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Sulphide in Soil	SPEC	6986221	N/A	2020/10/06	Sonya Radvan

**BV Labs ID:** NTH506 Dup2  
**Sample ID:** BH20-5D SS10  
**Matrix:** Soil

**Collected:** 2020/09/23  
**Shipped:**  
**Received:** 2020/09/28

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Sulphide in Soil	SPEC	6986221	N/A	2020/10/06	Sonya Radvan

**BV Labs ID:** NTH506 Dup3  
**Sample ID:** BH20-5D SS10  
**Matrix:** Soil

**Collected:** 2020/09/23  
**Shipped:**  
**Received:** 2020/09/28

Test Description	Instrumentation	Batch	Extracted	Date Analyzed	Analyst
Sulphide in Soil	SPEC	6986221	N/A	2020/10/06	Sonya Radvan



BV Labs Job #: COP3558  
Report Date: 2020/10/07

McClymont & Rak Engineers Inc  
Client Project #: 4842

### GENERAL COMMENTS

Each temperature is the average of up to three cooler temperatures taken at receipt

Package 1	1.7°C
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Sample NTH506 [BH20-5D SS10] : Sample was analyzed past method specified hold time for Sulphide.

**Results relate only to the items tested.**

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VERITAS

BV Labs Job #: COP3558

Report Date: 2020/10/07

## QUALITY ASSURANCE REPORT

McClymont &amp; Rak Engineers Inc

Client Project #: 4842

QC Batch	Parameter	Date	Matrix Spike		SPIKED BLANK		Method Blank	
			% Recovery	QC Limits	% Recovery	QC Limits	Value	UNITS
6974855	Soluble (20:1) Chloride (Cl <sup>-</sup> )	2020/10/01	NC	70 - 130	103	70 - 130	<20	ug/g
6974862	Soluble (20:1) Sulphate (SO <sub>4</sub> )	2020/10/01	NC	70 - 130	104	70 - 130	<20	ug/g
6976515	Available (CaCl <sub>2</sub> ) pH	2020/10/01			100	97 - 103		
6976739	Conductivity	2020/10/02			102	90 - 110	<2	umho/cm
6986220	Moisture-Subcontracted	2020/10/06					<0.30	%
6986221	Sulphide	2020/10/06	79 (1)	75 - 125	87	75 - 125	<0.5	mg/kg

Matrix Spike: A sample to which a known amount of the analyte of interest has been added. Used to evaluate sample matrix interference.

Spiked Blank: A blank matrix sample to which a known amount of the analyte, usually from a second source, has been added. Used to evaluate method accuracy.

Method Blank: A blank matrix containing all reagents used in the analytical procedure. Used to identify laboratory contamination.

NC (Matrix Spike): The recovery in the matrix spike was not calculated. The relative difference between the concentration in the parent sample and the spike amount was too small to permit a reliable recovery calculation (matrix spike concentration was less than the native sample concentration)

(1) Matrix Spike Parent ID [NTH506-01]



### VALIDATION SIGNATURE PAGE

The analytical data and all QC contained in this report were reviewed and validated by the following individual(s).

Antonella Brasil, Senior Project Manager

Anastassia Hamanov, Scientific Specialist

Ghayasuddin Khan, M.Sc., P.Chem., QP, Scientific Specialist, Inorganics

Veronica Falk, B.Sc., P.Chem., QP, Scientific Specialist, Organics

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BV Labs has procedures in place to guard against improper use of the electronic signature and have the required "signatories", as per ISO/IEC 17025, signing the reports.  
For Service Group specific validation please refer to the Validation Signature Page.

Client: Bureau Veritas Canada (2019) Inc.  
6740 Campobello Road  
Mississauga, ON  
L5N 2L8  
Attention: Antonella Brasil  
PO#:  
Invoice to: Bureau Veritas Canada (2019) Inc.

Report Number: 1939814  
Date Submitted: 2020-10-01  
Date Reported: 2020-10-07  
Project: C0P3558  
COC #: 863691

Page 1 of 3

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**Dear Antonella Brasil:**

**Please find attached the analytical results for your samples. If you have any questions regarding this report, please do not hesitate to call (613-727-5692).**

Report Comments:

APPROVAL: \_\_\_\_\_

Addrine Thomas, Inorganics Supervisor

All analysis is completed at Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) unless otherwise indicated.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by CALA, Canadian Association for Laboratory Accreditation to ISO/IEC 17025 for tests which appear on the scope of accreditation. The scope is available at: <http://www.cala.ca/scopes/2602.pdf>.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is licensed by the Ontario Ministry of the Environment, Conservation, and Parks (MECP) for specific tests in drinking water (license #2318). A copy of the license is available upon request.

Eurofins Environment Testing Canada Inc. (Ottawa, Ontario) is accredited by the Ontario Ministry of Agriculture, Food, and Rural Affairs for specific tests in agricultural soils.

Please note: Field data, where presented on the report, has been provided by the client and is presented for informational purposes only. Guideline values listed on this report are provided for ease of use (informational purposes) only. Eurofins recommends consulting the official provincial or federal guideline as required. Unless otherwise stated, measurement uncertainty is not taken into account when determining guideline or regulatory exceedances.



## Certificate of Analysis

Client: Bureau Veritas Canada (2019) Inc.  
6740 Campobello Road  
Mississauga, ON  
L5N 2L8  
Attention: Antonella Brasil  
PO#:  
Invoice to: Bureau Veritas Canada (2019) Inc.

Report Number: 1939814  
Date Submitted: 2020-10-01  
Date Reported: 2020-10-07  
Project: C0P3558  
COC #: 863691

					Lab I.D. Sample Matrix Sample Type Sampling Date Sample I.D.
Group	Analyte	MRL	Units	Guideline	1519615 Soil  2020-09-23 NTH506-BH20-5D SS10
Redox Potential	REDOX Potential		mV		181.6

**Guideline =**                      **\* = Guideline Exceedence**

Results relate only to the parameters tested on the samples submitted.  
Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range

## Certificate of Analysis

Client: Bureau Veritas Canada (2019) Inc.  
6740 Campobello Road  
Mississauga, ON  
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Report Number: 1939814  
Date Submitted: 2020-10-01  
Date Reported: 2020-10-07  
Project: C0P3558  
COC #: 863691

### QC Summary

Analyte	Blank	QC % Rec	QC Limits
<b>Run No</b> 390500 <b>Analysis/Extraction Date</b> 2020-10-07 <b>Analyst</b> R_R <b>Method</b> C SM2580B			
REDOX Potential	191 mV	101	

**Guideline =**                      \* = **Guideline Exceedence**

Results relate only to the parameters tested on the samples submitted.  
Methods references and/or additional QA/QC information available on request.

MRL = Method Reporting Limit, AO = Aesthetic Objective, OG = Operational Guideline, MAC = Maximum Acceptable Concentration, IMAC = Interim Maximum Acceptable Concentration, STD = Standard, PWQO = Provincial Water Quality Guideline, IPWQO = Interim Provincial Water Quality Objective, TDR = Typical Desired Range



6740 Campobello Road, Mississauga, Ontario L5N 2L8  
Phone: 905-817-5700 Fax: 905-817-5779 Toll Free: 800-563-6266  
CAM FCD-01191/6

CHAIN OF CUSTODY RECORD **152751** Page 1 of 1

Invoice Information		Report Information (if differs from invoice)		Project Information (where applicable)		Turnaround Time (TAT) Required			
Company Name: <u>McCLYMONT &amp; RAK</u>	Company Name:	Quotation #:	<input checked="" type="checkbox"/> Regular TAT (5-7 days) Most analyses						
Contact Name: <u>SALMAN</u>	Contact Name:	P.O. #/ AFE#:	PLEASE PROVIDE ADVANCE NOTICE FOR RUSH PROJECTS						
Address: <u>ZENWAY</u>	Address:	Project #: <u>4842</u>	Rush TAT (Surcharges will be applied)						
Address: <u>VAUGHAN</u>	Address:	Site Location:	<input type="checkbox"/> 1 Day <input type="checkbox"/> 2 Days <input type="checkbox"/> 3-4 Days						
Phone: <u>675-0160</u> Fax:	Phone: Fax:	Site #:	Date Required:						
Email: <u>starassoli@macrak.com</u>	Email:	Site Location Province: <u>PL</u>	Rush Confirmation #:						
MOE REGULATED DRINKING WATER OR WATER INTENDED FOR HUMAN CONSUMPTION MUST BE SUBMITTED ON THE BUREAU VERITAS LABORATORIES' DRINKING WATER CHAIN OF CUSTODY				Sampled By: <u>PL</u>					
<b>Regulation 153</b>		<b>Other Regulations</b>		<b>Analysis Requested</b>		<b>LABORATORY USE ONLY</b>			
<input type="checkbox"/> Table 1 <input type="checkbox"/> Res/Park <input type="checkbox"/> Med/ Fine	<input type="checkbox"/> CCME <input type="checkbox"/> Sanitary Sewer Bylaw	# OF CONTAINERS SUBMITTED		FIELD FILTERED (CIRCLE) Metals / Hg / CrVI		CUSTODY SEAL (Y/N)		COOLER TEMPERATURES	
<input type="checkbox"/> Table 2 <input type="checkbox"/> Ind/Comm <input type="checkbox"/> Coarse	<input type="checkbox"/> MISA <input type="checkbox"/> Storm Sewer Bylaw								
<input type="checkbox"/> Table 3 <input type="checkbox"/> Agri/ Other	<input type="checkbox"/> PW/QO Region								
<input type="checkbox"/> Table	<input type="checkbox"/> Other (Specify)								
FOR RSC (PLEASE CIRCLE) <u>RES</u>									
		<input type="checkbox"/> REG 406 Table							
Include Criteria on Certificate of Analysis: Y / N									
SAMPLES MUST BE KEPT COOL (< 10 °C) FROM TIME OF SAMPLING UNTIL DELIVERY TO BUREAU VERITAS									
SAMPLE IDENTIFICATION		DATE SAMPLED (YYYY/MM/DD)	TIME SAMPLED (HH:MM)	MATRIX					
1 <u>BH20-5D SS10</u>	<u>SEP. 23</u>		<u>SOIL</u>						
2									
3									
4									
5									
6									
7									
8									
9									
10									
RELINQUISHED BY: (Signature/Print)		DATE: (YYYY/MM/DD)	TIME: (HH:MM)	RECEIVED BY: (Signature/Print)		DATE: (YYYY/MM/DD)	TIME: (HH:MM)	BV JOB #	
<u>MCR</u>		<u>SEP. 28/20</u>	<u>12p</u>	<u>BV Antonella</u>		<u>2020-10-27</u>	<u>16:30</u>		

Unless otherwise agreed to in writing, work submitted on this Chain of Custody is subject to Bureau Veritas Laboratories' standard Terms and Conditions. Signing of this Chain of Custody document is acknowledgment and acceptance of our terms available at <http://www.bvlabs.com/terms-and-conditions>

COC-1004 (06/19)